## LM97593

## Dual ADC / Digital Tuner / AGC

## General Description

The LM97593 Dual ADC / Digital Tuner / AGC IC is a two channel digital downconverter (DDC) with integrated 12-bit analog-to-digital converters (ADCs) and automatic gain control (AGC). The LM97593 further enhances National's Diversity Receiver Chipset (DRCS) by integrating a wide-bandwidth dual ADC core with the DDC. The complete DRCS includes one LM97593 Dual ADC / Digital Tuner / AGC and two CLC5526 digitally controlled variable gain amplifiers (DVGAs). This system allows direct IF sampling of signals up to 300 MHz for enhanced receiver performance and reduced system costs. A block diagram for a DRCS-based narrowband communications system is shown in Figure 1.
The LM97593 offers high dynamic range digital tuning and filtering based on hard-wired digital signal processing (DSP) technology. Each channel has independent tuning, phase offset, filter coefficients, and gain settings. Channel filtering is performed by a series of three filters. The first is a 4 -stage Cascaded Integrator Comb (CIC) filter with a programmable decimation ratio from 8 to 2048. Next there are two symmetric FIR filters, a 21-tap and a 63-tap, both with independent programmable coefficients. The first FIR filter decimates the data by 2, the second FIR decimates by either 2 or 4 . Channel filter bandwidth at 52MSPS ranges from $\pm 650 \mathrm{kHz}$ down to $\pm 1.3 \mathrm{kHz}$. At 65MSPS, the maximum bandwidth increases to $\pm 812 \mathrm{kHz}$.
The LM97593's AGC controller monitors the ADC output and controls the ADC input signal level by adjusting the DVGA setting. AGC threshold, deadband+hysteresis, and the loop time constant are user defined. Total dynamic range of greater than 123dB full-scale signal to noise in a 200 kHz bandwidth can be achieved with the Diversity Receiver Chipset.

## Features

- $100 \%$ Software compatible with the CLC5903
- Pin compatible with the CLC5903 except for the analog input and reference section
- 123 dB dynamic range with CLC5526 DVGA (200kHz)
- On-chip precision reference
- User Programmable AGC with enhanced Power Detector
- Channel Filters include a Fourth Order CIC followed by 21tap and 63-tap Symmetric FIRs
- Flexible output formats
- Serial and Parallel output ports
- JTAG Boundary Scan
- 8-bit Microprocessor Interface
- 128 pin PQFP


## Key Specifications

- Internal ADC Resolution
- Sample Rate
- SNR ( $\mathrm{f}_{\mathbb{I}}=250 \mathrm{MHz}, 11$-bit, Nyquist)
- SNR ( $\mathrm{f}_{\mathrm{IN}}=250 \mathrm{MHz}, 200 \mathrm{kHz}$ )
- SFDR ( $\mathrm{f}_{\mathrm{IN}}=250 \mathrm{MHz}, 11$-bit, Nyquist)
- Full Power Bandwidth
- Power Consumption (65MSPS)


## Applications

- Cellular Basestations
- GSM / GPRS / EDGE / GSM Phase 2 Receivers
- Satellite Receivers
- Wireless Local Loop Receivers
- Digital Communications


## Block Diagram 1



FIGURE 1. Diversity Receiver Chipset Block Diagram

## Connection Diagram



FIGURE 2. LM97593VH PQFP Pinout

## Ordering Information

| Industrial ( $\mathbf{- 4 \mathbf { 0 0 } ^ { \circ } \mathbf { C } \text { to } \mathbf { + 8 5 } ^ { \circ } \mathbf { C } \text { ) }}$ Package |  |
| :---: | :---: |
| LM97593VH | 128 Pin PQFP |
| LM97593EB | Evaluation Board |

## Block Diagram 2



FIGURE 3. LM97593 Block Diagram

## Pin Descriptions and Equivalent Circuits

| Pin No. | Symbol | Equivalent Circuit | Description |
| :---: | :---: | :---: | :---: |
| ANALOG I/O |  |  |  |
| 13 27 | $\begin{aligned} & \mathrm{V}_{\mathrm{IN}} \mathrm{~A}- \\ & \mathrm{V}_{\mathrm{IN}} \mathrm{~B}- \end{aligned}$ | Analog Input | Negative differential input signal for the 'A' channel Negative differential input signal for the ' B ' channel |
| $\begin{array}{r}14 \\ 26 \\ \hline\end{array}$ | $\begin{aligned} & \mathrm{V}_{\text {IN }} \mathrm{A}+ \\ & \mathrm{V}_{\text {IN }} \mathrm{B}+ \end{aligned}$ | Analog Input | Positive differential input signal for the 'A' channel Positive differential input signal for the 'B' channel |
| 21 | $\mathrm{V}_{\text {REF }}$ | Control / Analog Input | Reference Select Pin / External Reference Voltage Input Input differential full scale swing $=2$ * $V_{\text {REF }}$ $\begin{array}{ll} \mathrm{V}_{\text {REF }}=\mathrm{V}_{\mathrm{A}} \text { to } \mathrm{V}_{\mathrm{A}}-0.3 \mathrm{~V}: & \text { Reference Voltage }=1.0 \mathrm{~V} \text { (Internal) } \\ \mathrm{V}_{\text {REF }}=0.8 \mathrm{~V} \text { to } 1.5 \mathrm{~V}: & \text { Refence Voltage }=\mathrm{V}_{\text {REF }} \text { (External) } \\ \hline \end{array}$ |
| $\begin{aligned} & 15 \\ & 24 \end{aligned}$ | $\begin{aligned} & \mathrm{v}_{\text {сом }} \mathrm{A} \\ & \mathrm{v}_{\text {сом }} \mathrm{B} \end{aligned}$ | Analog Output | Common Mode reference voltage for the ' A ' channel Common Mode reference voltage for the ' B ' channel These pins may be loaded to 1 mA for use as temperature stable 1.5 V references. |
| $\begin{aligned} & 16 \\ & 23 \end{aligned}$ | $\begin{aligned} & \mathrm{V}_{\mathrm{RP}} \mathrm{~A} \\ & \mathrm{~V}_{\mathrm{RP}} \mathrm{~B} \end{aligned}$ | Analog Output | Upper reference voltage for the 'A' channel Upper reference voltage for the ' $B$ ' channel |
| $\begin{aligned} & \hline 17 \\ & 22 \end{aligned}$ | $\begin{aligned} & \mathrm{V}_{\mathrm{RN}} \mathrm{~A} \\ & \mathrm{~V}_{\mathrm{RN}} \mathrm{~B} \end{aligned}$ | Analog Output | Lower reference voltage for the 'A' channel Lower reference voltage for the 'B' channel |
| 8 | REFSEL/DCS | Control Input | This is a three-state pin. $\mathrm{V}_{\text {COM }}=\mathrm{V}_{\text {COM }} \mathrm{A}$ or $\mathrm{V}_{\text {COM }} \mathrm{B}$. <br> REFSEL/DCS = AGND: the internal reference is enabled and duty cycle correction is applied to the ADC input clock (CK). <br> REFSEL/DCS $=\mathrm{V}_{\text {Сом }}$ : the internal reference is enabled and no duty cycle correction is applied to the ADC input clock (CK). <br> REFSEL/DCS $=\mathrm{V}_{\mathrm{A}}$ : DCS is on, the internal reference is disabled. Apply A 0.8-1.2V external reference to the $\mathrm{V}_{\text {REF }} \mathrm{pin}$. |
| DIGITAL I/O |  |  |  |
| 30 | PD | Input | POWER DOWN, when high both ADCs are powered down, when low, both ADCs are enabled |
| 45 | $\overline{\mathrm{MR}}$ | Input | MASTER RESET, Active Iow <br> Resets all registers within the chip. $\overline{\text { ASTROBE }}$ and $\overline{\text { BSTROBE }}$ are asserted during $\overline{\mathbf{M R}}$. |
| $\begin{array}{\|l\|} 82 \\ 78 \end{array}$ | $\begin{array}{\|l\|l\|} \text { AOUT } \\ \text { BOUT } \end{array}$ | Output | SERIAL OUTPUT DATA, Active high <br> The 2's complement serial output data is transmitted on these pins, MSB first. The output bits change on the rising edge of SCK (falling edge if SCK_POL=1) and should be captured on the falling edge of SCK (rising if SCK_POL=1). These pins are tri-stated at power up and are enabled by the SOUT_EN control register bit. See Figure 13 and Figure 34 timing diagrams. In Debug Mode AOUT=DEBUG[1], BOUT=DEBUG[0]. |
| $\begin{aligned} & \hline 127: 125 \\ & 40: 42 \end{aligned}$ | $\begin{aligned} & \text { AGAIN[2:0] } \\ & \text { BGAIN[2:0] } \end{aligned}$ | Output | OUTPUT DATA TO DVGA, Active high <br> 3 bit bus that sets the gain of the DVGA determined by the AGC circuit. |
| $\begin{aligned} & 124 \\ & 43 \end{aligned}$ | $\overline{\overline{\text { ASTROBE }}} \overline{\overline{\text { BSTROBE }}}$ | Output | DVGA STROBE, Active Iow <br> Strobes the data into the DVGA. See Figure 7 and Figure 41 timing diagrams. |
| 80 | SCK | Output | SERIAL DATA CLOCK, Active high or low <br> The serial data is clocked out of the chip by this clock. The active edge of the clock is user programmable. This pin is tri-stated at power up and is enabled by the SOUT_EN control register bit. See Figure 13 and Figure 34 timing diagrams. In Debug Mode outputs an appropiate clock for the debug data. If RATE=0 the input CK duty cycle will be reflected to SCK. |


| Pin No. | Symbol | Equivalent Circuit | Description |
| :---: | :---: | :---: | :---: |
| 99 | SCK_IN | Input | SERIAL DATA CLOCK INPUT, Active high or low <br> Data bits from a serial daisy-chain slave are clocked into a serial daisychain master on the falling edge of SCK_IN (rising if SCK_POL=1 on the slave). Tie low if not used. |
| 81 | SFS | Output | SERIAL FRAME STROBE, Active high or low <br> The serial word strobe. This strobe delineates the words within the serial output streams. This strobe is a pulse at the beginning of each serial word (PACKED=0) or each serial word I/Q pair (PACKED=1). The polarity of this signal is user programmable. This pin is tri-stated at power up and is enabled by the SOUT_EN control register bit. See and timing diagrams. In Debug Mode SFS=DEBUG[2]. |
| $\begin{aligned} & 84,86: 88,90, \\ & 91,93: 97, \\ & 104: 106,108, \\ & 109 \end{aligned}$ | POUT[15:0] | Output | PARALLEL OUTPUT DATA, Active high <br> The output data is transmitted on these pins in parallel format. The POUT_SEL[2:0] pins select one of eight 16-bit output words. The POUT_EN pin enables these outputs. POUT[15] is the MSB. In Debug Mode POUT[15:0]=DEBUG[19:4]. |
| 112:114 | POUT_SEL[2:0] | Input | PARALLEL OUTPUT DATA SELECT, Active high <br> The 16-bit output word is selected with these 3 pins according to . Not used in Debug Mode. For a serial daisy-chain master, POUT_SEL [2:0] become inputs from the slave: POUT_SEL[2]=SFS SLAVE , POUT_SEL[1]=BOUT SLAVE , and POUT_SEL[0]=AOUT SLAVE. . Tie low if not used. |
| 111 | $\overline{\text { POUT_EN }}$ | Input | PARALLEL OUTPUT ENABLE. Active Iow This pin enables the chip to output the selected output word on the POUT[15:0] pins. Not used in Debug Mode. Tie high if not used. |
| 77 | RDY | Output | READY FLAG, Active high or low <br> The chip asserts this signal to identify the beginning of an output sample period (OSP). The polarity of this signal is user programmable. This signal is typically used as an interrupt to a DSP chip, but can also be used as a start pulse to dedicated circuitry. This pin is active regardless of the state of SOUT_EN. In Debug Mode RDY=DEBUG[3]. |
| 37 | CK | Input | INPUT CLOCK. Active high <br> The clock input to the chip. The The $\mathbf{V}_{\mathbf{I N}} \mathbf{A}$ and $\mathbf{V}_{\mathbf{I N}} \mathbf{B}$ analog input signals are sampled on the rising edge of this signal. $\overline{\text { SII }}$ is clocked into the chip on the rising edge of CK. |
| 46 | SI | Input | SYNC IN. Active Iow <br> The sync input to the chip. The decimation counters, dither, and NCO phase can be synchronized by $\overline{\mathbf{S l}}$. This sync is clocked into the chip on the rising edge of CK. Tie this pin high if external sync is not required. All sample data is flushed by $\overline{\mathbf{S I}}$. To properly initialize the DVGA $\overline{\text { ASTROBE }}$ and $\overline{\text { BSTROBE }}$ are asserted during $\overline{\text { SI }}$. |
| $\begin{aligned} & 62,63,69: 73 \\ & 75 \end{aligned}$ | D[7:0] | Input/Output | DATA BUS. Active high <br> This is the 8 bit control data I/O bus. Control register data is loaded into the chip or read from the chip through these pins. The chip will only drive output data on these pins when $\overline{\mathbf{C E}}$ is low, $\overline{\mathbf{R D}}$ is low, and $\overline{\mathbf{W R}}$ is high. |
| 48, 50, 52:57 | A[7:0] | Input | ADDRESS BUS. Active high <br> These pins are used to address the control registers within the chip. Each of the control registers within the chip are assigned a unique address. A control register can be written to or read from by setting A [7:0] to the register's address and setting $\overline{\mathrm{CE}}, \overline{\mathrm{RD}}$, and $\overline{\mathrm{WR}}$ appropriately. |
| 59 | $\overline{\mathrm{RD}}$ | Input | READ ENABLE. Active Iow <br> This pin enables the chip to output the contents of the selected register on the $\mathrm{D}[7: 0]$ pins when $\overline{\mathrm{CE}}$ is also low. |


| Pin No. | Symbol | Equivalent Circuit | Description |
| :---: | :---: | :---: | :---: |
| 58 | $\overline{W R}$ | Input | WRITE ENABLE. Active low <br> This pin enables the chip to write the value on the $\mathbf{D}[7: 0]$ pins into the selected register when $\overline{\mathrm{CE}}$ is also low. This pin can also function as $\mathbf{R D} / \overline{\mathbf{C E}}$ if RD is held low. See for details. |
| 60 | $\overline{\mathrm{CE}}$ | Input | CHIP ENABLE. Active Iow <br> This control strobe enables the read or write operation. The contents of the register selected by $\mathbf{A}[7: 0]$ will be output on $\mathbf{D}[7: 0]$ when $\overline{\mathbf{R D}}$ is low and $\overline{\mathbf{C E}}$ is low. If $\overline{\mathbf{W R}}$ is low and $\overline{\mathbf{C E}}$ is low, then the selected register will be loaded with the contents of $\mathrm{D}[7: 0]$. |
| 116 | TDO | Output | TEST DATA OUT. Active high |
| 117 | TDI | Input | TEST DATA IN. Active high with pull-up |
| 118 | TMS | Input | TEST MODE SELECT. Active high with pull-up |
| 119 | TCK | Input | TEST CLOCK. Active high. Tie low if JTAG is not used. |
| 121 | TRST | Input | TEST RESET. Active low with pull-up Asynchronous reset for TAP controller. Tie low or to $\overline{\mathbf{M R}}$ if JTAG is not used. |
| 122 | SCAN_EN | Input | SCAN ENABLE. Active Iow with pull-up <br> Enables access to internal scan registers. Tie high. Used for manufacturing test only! |
| Digital Power Supplies |  |  |  |
| $\begin{aligned} & \hline 38,39,64, \\ & 79,92,102, \\ & 107,128 \end{aligned}$ | $\mathrm{V}_{\mathrm{DR}}$ | DDC Output Driver Power | I/O Power Supply, 3.3V nominal. Quantity 8. |
| $\begin{aligned} & 1,47,61,68, \\ & 83,89,98, \\ & 110 \end{aligned}$ | DRGND | DDC Output Driver Ground | I/O Ground Return. Quantity 8. |
| $\begin{aligned} & \hline 49,74,85, \\ & 115,123 \end{aligned}$ | $\mathrm{V}_{\mathrm{D} 18}$ | DDC Core Power | DSP Digital Core Power Supply, 1.8V nominal. Quantity 5. |
| $\begin{aligned} & \hline 49,74,85, \\ & 115,123 \end{aligned}$ | $\mathrm{V}_{\mathrm{D} 18}$ | DDC Core Power | DSP Digital Core Power Supply, 1.8V nominal. Quantity 5. |
| $\begin{aligned} & 44,51,65, \\ & 66,76,103, \\ & 120 \end{aligned}$ | D18GND | DDC Core Ground | DSP Digital Core Ground Return. Quantity 7. |
| 4, 6, 31, 34 | $\mathrm{V}_{\mathrm{D}}$ | ADC Digital Power | ADC Digital Logic Power Supply, 3.3V nominal. Quantity 4. |
| 5, 7, 32, 33 | DGND | ADC Digital Ground | ADC Digital Logic Ground Return. Quantity 4. |
| Analog Power Supplies |  |  |  |
| $\begin{aligned} & 10,11,19, \\ & 25,29 \end{aligned}$ | $\mathrm{V}_{\mathrm{A}}$ | ADC Analog Power | ADC Analog Power Supply, 3.3V nominal. Quantity 5. |
| $\begin{aligned} & 2,9,12,18, \\ & 20,28 \end{aligned}$ | AGND | ADC Analog Ground | ADC Analog Ground Return. Quantity 6. |
| Unconnected Pins |  |  |  |
| $\begin{aligned} & 3,35,36,67, \\ & 100,101 \end{aligned}$ | NC | NC | Not Connected. These pins should be left floating. |

## Absolute Maximum Ratings

(Notes 1, 2)
If Military/Aerospace specified devices are required, please contact the National Semiconductor Sales Office/ Distributors for availability and specifications.

| ADC Analog, Digital and IO Supply | -0.3 V to 4.2 V |
| :--- | ---: |
| Voltages $\left(\mathrm{V}_{\mathrm{A}}, \mathrm{V}_{\mathrm{D}}\right.$ and $\left.\mathrm{V}_{\mathrm{DR}}\right)$ |  |
| Difference between $\mathrm{V}_{\mathrm{A}}, \mathrm{V}_{\mathrm{D}}$, and $\mathrm{V}_{\mathrm{DR}}$ | $\leq 100 \mathrm{mV}$ |
| Positive Core Supply Voltage $\left(\mathrm{V}_{\mathrm{D} 18}\right)$ | -0.3 V to 2.35 V |
| Voltage on Any Input or Output Pin | -0.3 V to $\left(\mathrm{V}_{\mathrm{DR}}+0.3 \mathrm{~V}\right)$ |
| (Not to exceed 4.2V) | $\pm 5 \mathrm{~mA}$ |
| Input Current at Any Pin other than |  |
| Supply Pins (Note 3) | $\pm 50 \mathrm{~mA}$ |
| Package Input Current (Note 3) | $+125^{\circ} \mathrm{C}$ |
| Max Junction Temp $\left(\mathrm{T}_{\mathrm{J}}\right)$ | $39^{\circ} \mathrm{C} / \mathrm{W}$ |
| Thermal Resistance $\left(\theta_{\mathrm{JA}}\right)$ | 3.2 W |
| Package Dissipation at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ |  |
| (Note 4) |  |
| ESD Susceptibility (Note 5) | 2000 V |
| $\quad$ Human Body Model $(1.5 \mathrm{k} \Omega, 100 \mathrm{pF})$ | 200 V |
| Machine Model ( $0 \Omega, 200 \mathrm{pF})$ | 750 V |
| Charge Device Model | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |

Operating Ratings (Notes 1, 2)
Soldering process must comply with National Semiconductor's Reflow Temperature Profile specifications. Refer to www.national.com/packaging. (Note 6)
Operating Temperature
Range
ADC Analog, Digital and IO

$$
-40^{\circ} \mathrm{C} \leq \mathrm{T}_{\mathrm{A}} \leq+85^{\circ} \mathrm{C}
$$

Supply Voltages ( $\mathrm{V}_{\mathrm{A}}, \mathrm{V}_{\mathrm{D}}$ and
$\mathrm{V}_{\mathrm{DR}}$ )
Digital Core Supply Voltage
(VD18) $\quad+1.6 \mathrm{~V}$ to +2.0 V

Difference Between AGND, DGND, DRGND and D18GND $\leq 100 \mathrm{mV}$ Voltage on Any Input or Output Pin

0 V to +3.3 V
$V_{C M}$
1.0 V to 2.0 V
$30 \%$ to 70 \%

## Reliability Information

Transistor Count

## LM97593 Electrical Characteristics

Unless otherwise specified, the following specifications apply: AGND = DGND = DRGND = D18GND = OV, $V_{A}=V_{D}=V_{D R}=+3.3 \mathrm{~V}$, $\mathrm{V}_{\mathrm{D} 18}=+1.8 \mathrm{~V}$, Internal $\mathrm{V}_{\mathrm{REF}}=+1.0 \mathrm{~V}, \mathrm{f}_{\mathrm{CLK}}=65 \mathrm{MHz}, \mathrm{V}_{\mathrm{CM}}=\mathrm{V}_{\mathrm{COM}}, \mathrm{t}_{\mathrm{R}}=\mathrm{t}_{\mathrm{F}}=1 \mathrm{~ns}, \mathrm{C}_{\mathrm{L}}=5 \mathrm{pF} /$ pin. The ADC's 11 most significant bits observed at the mixer output debug tap with $\mathrm{NCO}=0 \mathrm{~Hz}$. Typical values are for $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$. Boldface limits apply for $\mathrm{T}_{\text {MIN }} \leq \mathrm{T}_{\mathrm{A}}$ $\leq \mathrm{T}_{\text {MAX }}$. All other limits apply for $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$. (Notes 7, 8, 9)

| Symbol | Parameter | Conditions | Typical (Note 10) | Limits | Units (Limits) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| STATIC CONVERTER CHARACTERISTICS |  |  |  |  |  |
|  | Resolution with No Missing Codes |  |  | 11 | Bits (min) |
| INL | Integral Non Linearity (Note 11) | Ramp, End Point | $\pm 0.7$ | $\begin{gathered} 2 \\ -2 \end{gathered}$ | $\begin{aligned} & \text { LSB (max) } \\ & \text { LSB (min) } \end{aligned}$ |
| DNL | Differential Non Linearity | Ramp, End Point | $\pm 0.3$ | $\begin{gathered} \hline 0.85 \\ -0.85 \\ \hline \end{gathered}$ | $\begin{aligned} & \text { LSB ( } \max ) \\ & \text { LSB }(\min ) \\ & \hline \end{aligned}$ |
| $\mathrm{V}_{\text {OFF }}$ | Offset Error | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | -4.1 |  | LSB |

REFERENCE AND ANALOG INPUT CHARACTERISTICS

| $\mathrm{V}_{\mathrm{CM}}$ | Common Mode Input Voltage |  | 1.5 | 1.0 | V (min) |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | 2.0 | V (max) |
| $\begin{aligned} & \hline \mathrm{V}_{\text {сом }} \mathrm{A} \\ & \mathrm{~V}_{\text {сом }} \mathrm{B} \end{aligned}$ | Reference Output Voltage |  | 1.5 |  | V |
| $\mathrm{C}_{\text {IN }}$ | $\mathrm{V}_{\text {IN }}$ Input Capacitance (each pin to GND) $\left(\mathrm{V}_{\mathrm{IN}}=1.5 \mathrm{Vdc} \pm 0.5 \mathrm{~V}\right)$ (Note 12) | CK LOW | 8 |  | pF |
|  |  | CK HIGH | 7 |  | pF |
| $\mathrm{V}_{\text {REF }}$ | External Reference Voltage (Note 14) |  | 1.0 | 0.8 | V (min) |
|  |  |  |  | 1.2 | V (max) |
|  | Reference Input Resistance |  | 1 |  | $\mathrm{M} \Omega$ |

## DYNAMIC CONVERTER CHARACTERISTICS

| FPBW | Full Power Bandwidth |  | 650 |  | MHz |
| :--- | :--- | :--- | :--- | :--- | :---: |
| SNR |  | $\mathrm{f}_{\mathbb{N}}=20 \mathrm{MHz}, \mathrm{V}_{\mathbb{I N}}=-3 \mathrm{dBFS}$ | 66.2 |  | dBFS |
|  |  | $\mathrm{f}_{\mathbb{I}}=249 \mathrm{MHz}, \mathrm{V}_{\mathbb{I}}=-3 \mathrm{dBFS}$ | 63.7 |  | dBFS |
|  |  | $\mathrm{f}_{\mathbb{I N}}=249 \mathrm{MHz}, \mathrm{V}_{\mathbb{I}}=-9 \mathrm{dBFS}$ | 63.9 | $\mathbf{6 2 . 2}$ | $\mathrm{dBFS}(\mathrm{min})$ |


| Symbol | Parameter | Conditions | Typical (Note 10) | Limits | Units (Limits) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| SINAD | Signal-to-Noise and Distortion | $\begin{aligned} & \mathrm{f}_{\mathrm{IN}}=20 \mathrm{MHz}, \mathrm{~V}_{\mathrm{IN}} \\ &=-3 \mathrm{dBFS} \\ & \mathrm{f}_{\mathrm{IN}}=249 \mathrm{MHz}, \mathrm{~V}_{\mathrm{IN}}=-3 \mathrm{dBFS} \\ & \mathrm{f}_{\mathrm{IN}}=249 \mathrm{MHz}, \mathrm{~V}_{\mathrm{IN}}=-9 \mathrm{dBFS} \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 62.8 \\ & 62.0 \\ & 63.4 \end{aligned}$ | 60.4 | dBFS <br> dBFS <br> dBFS (min) |
| ENOB | Effective Number of Bits (Relative to Full Scale) | $\begin{aligned} & \mathrm{f}_{\mathrm{IN}}=20 \mathrm{MHz}, \mathrm{~V}_{\mathrm{IN}} \\ &=-3 \mathrm{dBFS} \\ & \mathrm{f}_{\mathrm{IN}}=249 \mathrm{MHz}, \mathrm{~V}_{\mathrm{IN}}=-3 \mathrm{dBFS} \\ & \mathrm{f}_{\mathrm{IN}}=249 \mathrm{MHz}, \mathrm{~V}_{\mathrm{IN}}=-9 \mathrm{dBFS} \end{aligned}$ | $\begin{aligned} & 10.6 \\ & 10.0 \\ & 10.3 \end{aligned}$ |  | Bits <br> Bits Bits (min) |
| THD | Total Harmonic Distortion | $\begin{aligned} & \hline \mathrm{f}_{\mathrm{IN}}=20 \mathrm{MHz}, \mathrm{~V}_{\mathrm{IN}} \\ &=-3 \mathrm{dBFS} \\ & \mathrm{f}_{\mathrm{IN}}=249 \mathrm{MHz}, \mathrm{~V}_{\mathrm{IN}}=-3 \mathrm{dBFS} \\ & \mathrm{f}_{\mathrm{IN}}=249 \mathrm{MHz}, \mathrm{~V}_{\mathrm{IN}}=-9 \mathrm{dBFS} \\ & \hline \end{aligned}$ | $\begin{aligned} & -77.1 \\ & -57.9 \\ & -64.6 \end{aligned}$ | -54.1 | $\begin{gathered} \mathrm{dBc} \\ \mathrm{dBc} \\ \mathrm{dBc}(\max ) \end{gathered}$ |
| H2 | Second Harmonic Distortion | $\begin{aligned} & \mathrm{f}_{\mathrm{IN}}=20 \mathrm{MHz}, \mathrm{~V}_{\mathrm{IN}} \\ &=-3 \mathrm{dBFS} \\ & \mathrm{f}_{\mathrm{IN}}=249 \mathrm{MHz}, \mathrm{~V}_{\mathrm{IN}}=-3 \mathrm{dBFS} \\ & \mathrm{f}_{\mathrm{IN}}=249 \mathrm{MHz}, \mathrm{~V}_{\mathrm{IN}}=-9 \mathrm{dBFS} \end{aligned}$ | $\begin{aligned} & -82.7 \\ & -59.9 \\ & -67.3 \end{aligned}$ | -59.3 | $\begin{gathered} \mathrm{dBc} \\ \mathrm{dBc} \\ \mathrm{dBc}(\max ) \end{gathered}$ |
| H3 | Third Harmonic Distortion | $\begin{aligned} & \hline \mathrm{f}_{\mathrm{IN}}=20 \mathrm{MHz}, \mathrm{~V}_{\mathrm{IN}} \\ &=-3 \mathrm{dBFS} \\ & \mathrm{f}_{\mathrm{IN}}=249 \mathrm{MHz}, \mathrm{~V}_{\mathrm{IN}}=-3 \mathrm{dBFS} \\ & \mathrm{f}_{\mathrm{IN}}=249 \mathrm{MHz}, \mathrm{~V}_{\mathrm{IN}}=-9 \mathrm{dBFS} \end{aligned}$ | $\begin{aligned} & -91.7 \\ & -69.0 \\ & -72.5 \end{aligned}$ | -56.8 | $\begin{gathered} \mathrm{dBc} \\ \mathrm{dBc} \\ \mathrm{dBc}(\mathrm{~min}) \end{gathered}$ |
| SFDR | Spurious Free Dynamic Range | $\begin{aligned} & \hline \mathrm{f}_{\mathrm{IN}}=20 \mathrm{MHz}, \mathrm{~V}_{\mathrm{IN}}=-3 \mathrm{dBFS} \\ & \mathrm{f}_{\mathrm{IN}}=249 \mathrm{MHz}, \mathrm{~V}_{\mathrm{IN}}=-3 \mathrm{dBFS} \\ & \mathrm{f}_{\mathrm{IN}}=249 \mathrm{MHz}, \mathrm{~V}_{\mathrm{IN}}=-9 \mathrm{dBFS} \end{aligned}$ | 79.7 |  | $\begin{gathered} \text { dBFS } \\ \text { dBFS (min) } \\ \text { dBFS } \end{gathered}$ |
|  |  |  | 68.0 |  |  |
|  |  |  | 76.3 | 67.0 |  |
| IMD | Intermodulation Distortion | $\begin{gathered} \mathrm{f}_{1 \mathrm{NN}}=246 \mathrm{MHz}, \mathrm{~V}_{\text {IN }}=-15 \mathrm{dBFS} \\ \mathrm{f}_{2 \mathrm{IN}}=250 \mathrm{MHz}, \mathrm{~V}_{\text {IN }}=-15 \mathrm{dBFS} \\ \left(\mathrm{f}_{1 \mathrm{~N}}+\mathrm{f}_{\text {2IN }}=-9 \mathrm{dBFS}\right) \end{gathered}$ | -77.5 |  | dBFS |
|  | Dynamic Gain Error | -3 dBFS reference, -50 dBFS target | $\pm 1.3$ | $\pm 2$ | dB |
| INTERCHANNEL CHARACTERISTICS |  |  |  |  |  |
|  | Channel - Channel Offset Match | $10 \mathrm{MHz}-1 \mathrm{dBFS}$ driven | $\pm 0.2$ |  | \%FS |
|  | Channel - Channel Gain Match | 10 MHz -1dBFS driven | $\pm 0.4$ |  | \%FS |
|  | Crosstalk (AGC fixed at 0dB gain, with AGC operating the crosstalk will improve at the output) | 249 MHz -3dBFS driven channel, $50 \Omega$ termination measured channel | 60(+42) (Note <br> 16) |  | dBc |
| CIC OUTPUT CHARACTERISTICS |  |  |  |  |  |
| SNR | Signal-to-Noise Ratio | CIC Decimation $=8, \mathrm{NCO}=$ <br> $11.1 \mathrm{MHz}(248.9 \mathrm{MHz}$ <br> @65MSPS aliases to 11.1 <br> $\mathrm{MHz}), \mathrm{f}_{\mathrm{IN}}=249 \mathrm{MHz}$ at -3 dBFS , <br> signal observed at F1 In Debug tap | 68.6 | 66.1 | dBFS |
| SINAD | Signal-to-Noise and Distortion |  | 68.5 | 66.1 | dBFS |
| SFDR | Spurious Free Dynamic Range |  | 75.1 | 70.3 | dBc |
| DDC OUTPUT CHARACTERISTICS |  |  |  |  |  |
| SNR | Signal-to-Noise Ratio | GSM Filter set, 200 kHz channel BW, NCO $=11.1 \mathrm{MHz}$ (248.9MHz @52MSPS aliases to 11.1 MHz ), $\mathrm{f}_{\mathrm{S}}=52 \mathrm{MSPS}$, $\mathrm{f}_{\mathrm{IN}}=249 \mathrm{MHz}$ at -9 dBFS | $\begin{gathered} \hline 82(+42) \text { (Note } \\ 16) \\ \hline \end{gathered}$ |  | dBFS |
| SINAD | Signal-to-Noise and Distortion |  | 73 |  | dBc |
| SFDR | Spurious Free Dynamic Range |  | 90 |  | dBc |
| SNR | Signal-to-Noise Ratio | GSM Filter set, 200 kHz channel BW, NCO $=11.1 \mathrm{MHz}$ (248.9MHz @52MSPS aliases to 11.1 MHz ), $\mathrm{f}_{\mathrm{S}}=52 \mathrm{MSPS}$, $\mathrm{f}_{\mathrm{IN}}=249 \mathrm{MHz}$ at -3 dBFS | $\begin{gathered} 76(+42) \text { (Note } \\ 16) \\ \hline \end{gathered}$ |  | dBFS |
| SINAD | Signal-to-Noise and Distortion |  | 74 |  | dBc |
| SFDR | Spurious Free Dynamic Range |  | 90 |  | dBc |
| SNR | Signal-to-Noise Ratio | GSM Filter set, 200 kHz channel BW, NCO $=11.1 \mathrm{MHz}$ (248.9MHz @65MSPS aliases to 11.1 MHz ), $\mathrm{f}_{\mathrm{S}}=65 \mathrm{MSPS}$, $\mathrm{f}_{\mathrm{IN}}=249 \mathrm{MHz}$ at -9 dBFS | $\begin{gathered} 79(+42) \text { (Note } \\ 16) \end{gathered}$ |  | dBFS |
| SINAD | Signal-to-Noise and Distortion |  | 71 |  | dBc |
| SFDR | Spurious Free Dynamic Range |  | 81 |  | dBc |


| Symbol | Parameter | Conditions | Typical <br> $($ Note 10$)$ | Limits | Units <br> (Limits) |
| :--- | :--- | :---: | :---: | :---: | :---: |
| SNR | Signal-to-Noise Ratio | GSM Filter set, 200 kHz <br> channel BW, NCO $=11.1 \mathrm{MHz}$ <br> $(248.9 \mathrm{MHz} \mathrm{@} \mathrm{65MSPS} \mathrm{aliases}$ <br> to 11.1 MHz$), \mathrm{f}_{\mathrm{S}}=65 \mathrm{MSPS}$, <br> $\mathrm{f}_{\mathrm{IN}}=249 \mathrm{MHz}$ at -3 dBFS | $742)($ Note <br> $16)$ | 71 | dBFS |
| SINAD | Signal-to-Noise and Distortion | 80 | dBc |  |  |
| SFDR | Spurious Free Dynamic Range |  | dBc |  |  |

## DC and Logic Electrical Characteristics

Unless otherwise specified, the following specifications apply: AGND = DGND = DRGND = D18GND = OV, $V_{A}=V_{D}=V_{D R}=+3.3 \mathrm{~V}$, $\mathrm{V}_{\mathrm{D} 18}=+1.8 \mathrm{~V}$, Internal $\mathrm{V}_{\mathrm{REF}}=+1.0 \mathrm{~V}, \mathrm{f}_{\mathrm{CLK}}=65 \mathrm{MHz}, \mathrm{V}_{\mathrm{CM}}=\mathrm{V}_{\mathrm{COM}}, \mathrm{t}_{\mathrm{R}}=\mathrm{t}_{\mathrm{F}}=\mathrm{TBD} \mathrm{ns}, \mathrm{C}_{\mathrm{L}}=5 \mathrm{pF} /$ pin. CIC Decimation $=48$, F 2 Decimation $=2$. Typical values are for $T_{A}=25^{\circ} \mathrm{C}$. Boldface limits apply for $T_{\text {MIN }} \leq T_{A} \leq T_{\text {MAX }}$. All other limits apply for $T_{A}=25^{\circ}$ C.

| Symbol | Parameter | Conditions | Typical <br> (Note 10) | Limits | Units <br> (Limits) |
| :--- | :--- | :--- | :---: | :---: | :---: |
| $\mathrm{V}_{\mathrm{IL}}$ | Voltage input low |  |  | $\mathbf{0 . 7}$ | $\mathrm{V}(\mathrm{max})$ |
| $\mathrm{V}_{\mathrm{IH}}$ | Voltage input high |  |  | $\mathbf{2 . 3}$ | $\mathrm{V}(\mathrm{min})$ |
| $\mathrm{I}_{\mathrm{OZ}}$ | Input current |  |  | $\mathbf{2 0}$ | $\mu \mathrm{A}$ |
| $\mathrm{V}_{\mathrm{OL}}$ | Voltage output low $\left(\mathrm{I}_{\mathrm{OL}}=7 \mathrm{~mA}\right)$ |  |  | $\mathbf{0 . 4}$ | $\mathrm{V}(\mathrm{max})$ |
| $\mathrm{V}_{\mathrm{OH}}$ | Voltage output high $\left(\mathrm{I}_{\mathrm{OH}}=-7 \mathrm{~mA}\right)$ |  |  | $\mathbf{2 . 4}$ | $\mathrm{V}(\mathrm{min})$ |
| $\mathrm{C}_{\mathrm{IN}}$ | Input capacitance |  | 5.0 | pF |  |

POWER SUPPLY CHARACTERISTICS

| $\mathrm{I}_{\mathrm{A}}$ | ADC Analog Supply Current | 65MSPS | 96 | 121 | mA (max) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{I}_{\mathrm{A}}$ | ADC Analog Supply Current | 52MSPS | 84 |  | mA |
| $\mathrm{I}_{\mathrm{D}}$ | ADC Digital Supply Current | 65MSPS | 24 | 28 | mA (max) |
| $\mathrm{I}_{\mathrm{D}}$ | ADC Digital Supply Current | 52MSPS | 20 |  | mA |
| $\mathrm{I}_{\mathrm{DR}}$ | Digital Output Supply Current (Note 15) | 65MSPS | 14 | 18 | mA (max) |
| $\mathrm{I}_{\mathrm{DR}}$ | Digital Output Supply Current (Note 15) | 52MSPS | 10 |  | mA |
| $\mathrm{I}_{\text {D18 }}$ | Digital Core Supply Current | 65MSPS | 67 | 78 | mA (max) |
| $\mathrm{I}_{\text {D18 }}$ | Digital Core Supply Current | 52MSPS | 53 |  | mA |
| $\mathrm{P}_{\text {D65 }}$ | Total Power Dissipation | GSM Set, 65MSPS | 560 | 793 | mW (max) |
| $\mathrm{P}_{\mathrm{D} 52}$ | Total Power Dissipation | GSM Set, 52MSPS | 485 |  | mW |
| PSRR | Power Supply Rejection Ratio | Rejection of Full-Scale Error with VA = 3.0 V vs. 3.6 V |  |  | dB |

## AC Electrical Characteristics

Unless otherwise specified, the following specifications apply: AGND = DGND = DRGND = D18GND = 0V, $\mathrm{V}_{\mathrm{A}}=\mathrm{V}_{\mathrm{D}}=\mathrm{V}_{\mathrm{DR}}=+3.3 \mathrm{~V}$ $( \pm 10 \%), \mathrm{V}_{\mathrm{D} 18}=+1.8 \mathrm{~V}( \pm 10 \%)$, Internal $\mathrm{V}_{\mathrm{REF}}=+1.0 \mathrm{~V}, \mathrm{f}_{\mathrm{CLK}}=65 \mathrm{MHz}, \mathrm{V}_{\mathrm{CM}}=\mathrm{V}_{\mathrm{COM}}, \mathrm{t}_{\mathrm{R}}=\mathrm{t}_{\mathrm{F}}=1 \mathrm{~ns}, \mathrm{C}_{\mathrm{L}}=5 \mathrm{pF} / \mathrm{pin}$. CIC Decimation $=$ 48, F2 Decimation $=2$. Typical values are for $T_{A}=25^{\circ} \mathrm{C}$. Boldface limits apply for $\mathrm{T}_{\text {MIN }} \leq \mathrm{T}_{\mathrm{A}} \leq \mathrm{T}_{\text {MAX }}$. All other limits apply for $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$. (Note 13)

| Symbol | Parameter ( $\left.\mathrm{C}_{\mathrm{L}}=50 \mathrm{pF}\right)$ | Min | Typical (Note 10) | Max | Units |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Clock Input |  |  |  |  |  |
| $\mathrm{F}_{\text {CK }}$ | Clock (CK) Frequency (Figure 6) | 20 |  | 65 | MHz |
| $\mathrm{t}_{\text {CKDC }}$ | CK duty cycle, DCS off (Figure 6) | 40 |  | 60 | \% |
| $\mathrm{t}_{\mathrm{RF}}$ | CK rise and fall times ( $\mathrm{V}_{\mathrm{IL}}$ to $\mathrm{V}_{\text {IH }}$ ) (Figure 6) |  |  | 2 | ns |
|  | NCO Tuning Resolution |  | 0.02 |  | Hz |
|  | NCO Phase Resolution |  | 0.005 |  | 0 |

## Control Interface

| $\mathrm{t}_{\text {MRA }}$ | $\overline{\mathrm{MR}}$ Active Time (Figure 4) | 4 |  | CK periods |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{t}_{\text {MRIC }}$ | $\overline{\text { MR }}$ Inactive to first Control Port Access (Figure 4) | 10 |  | CK periods |
| $\mathrm{t}_{\text {MRSU }}$ | $\overline{\mathbf{M R}}$ Setup Time to CK (Figure 4) | 6 |  | ns |
| $\mathrm{t}_{\text {MRH }}$ | $\overline{\text { MR Hold Time from CK (Figure 4) }}$ | 2 |  | ns |
| $\mathrm{t}_{\text {SISU }}$ | $\overline{\text { SI S Setup Time to CK (Figure 5) }}$ | 6 |  | ns |
| $\mathrm{t}_{\text {SIH }}$ | SI Hold Time from CK (Figure 5) | 2 |  | ns |
| $\mathrm{t}_{\text {SIW }}$ | $\overline{\text { SI Pulse Width (Figure 5) }}$ | 4 |  | CK periods |
| DVGA Interface |  |  |  |  |
| $\mathrm{t}_{\text {STIW }}$ | AlBSTROBE Inactive Pulse Width (Figure 7) |  | 2 | CK periods |
| $\mathrm{t}_{\text {GSTB }}$ | $\overline{\text { AlBGAIN }}$ setup before $\overline{\text { AlBSTROBE (Figure 7) }}$ | 6 |  | ns |

## Parallel Output Interface

| $t_{\text {OENV }}$ | POUT_EN Active to POUT[15:0] Valid (Figure 9) |  | $\mathbf{1 2}$ | ns |
| :--- | :--- | :--- | :--- | :---: |
| $\mathrm{t}_{\text {OENT }}$ | POUT_EN Inactive to POUT[15:0] Tri-State (Figure 9) |  |  | $\mathbf{1 0}$ |
| $\mathrm{t}_{\text {SELV }}$ | PSEL[2:0] to POUT[15:0] Valid (Figure 10) |  | ns |  |
| $\mathrm{t}_{\text {POV }}$ | RDY to POUT[15:0] New Value Valid (Note 5) (Figure 11) |  | $\mathbf{1 3}$ | ns |
| $\mathrm{t}_{\text {DBG }}$ | SCK to POUT[15:0], RDY, SFS, AOUT, BOUT Valid (Figure 12) |  | $\mathbf{7}$ | ns |

## Serial Interface

| $t_{\text {SFSV }}$ | SCK to SFS Valid (Note 3) (Figure 13) | $\mathbf{- 2}$ | 1.6 | $\mathbf{3 . 5}$ | ns |
| :--- | :--- | :---: | :---: | :---: | :---: |
| $\mathrm{t}_{\mathrm{OV}}$ | SCK to AIBOUT Valid (Note 4) (Figure 13) | $\mathbf{- 2}$ | 1.7 | $\mathbf{3 . 5}$ | ns |
| $\mathrm{t}_{\mathrm{RDYW}}$ | RDY Pulse Width (Figure 13) |  | $\mathbf{2}$ |  | CK periods |
| $\mathrm{t}_{\mathrm{DCMSU}}$ | PSEL[2:0] Setup Time to SCK_IN (Figure 8) | $\mathbf{3}$ | 1.4 |  | ns |
| $\mathrm{t}_{\mathrm{DCMH}}$ | PSEL[2:0] Hold Time from SCK_IN (Figure 8) | $\mathbf{0 . 5}$ | -0.9 |  | ns |
| $\mathrm{t}_{\mathrm{RDYV}}$ | SCK to RDY valid (Figure 13) | $\mathbf{- 3}$ | 1.8 | $\mathbf{4}$ | ns |

JTAG Interface

| $\mathrm{t}_{\text {JPCO }}$ | Propagation Delay TCK to TDO (Figure 14) |  |  | $\mathbf{2 5}$ |
| :--- | :--- | :---: | :---: | :---: |
| $\mathrm{t}_{\mathrm{JSCO}}$ | Propagation Delay TCK to Data Out (Figure 14) |  | ns |  |
| $\mathrm{t}_{\mathrm{JPDZ}}$ | Disable Time TCK to TDO (Figure 14) |  | $\mathbf{3 5}$ | ns |
| $\mathrm{t}_{\text {JSDZ }}$ | Disable Time TCK to Data Out (Figure 14) |  | $\mathbf{2 5}$ | ns |
| $\mathrm{t}_{\text {JPEN }}$ | Enable Time TCK to TDO (Figure 14) | $\mathbf{0}$ | $\mathbf{3 5}$ | ns |
| $\mathrm{t}_{\text {JSEN }}$ | Enable Time TCK to Data Out (Figure 14) | $\mathbf{0}$ |  | $\mathbf{2 5}$ |
| $\mathrm{t}_{\text {JSSU }}$ | Setup Time Data to TCK (Figure 14) | $\mathbf{1 0}$ |  | ns |
| $\mathrm{t}_{\mathrm{JPSU}}$ | Setup Time TDI, TMS to TCK (Figure 14) | $\mathbf{1 0}$ |  | ns |
| $\mathrm{t}_{\text {JSH }}$ | Hold Time Data to TCK (Figure 14) | $\mathbf{4 5}$ |  | ns |
| $\mathrm{t}_{\text {JPH }}$ | Hold Time TCK to TDI, TMS (Figure 14) | $\mathbf{4 5}$ |  | ns |
| $\mathrm{t}_{\mathrm{JCH}}$ | TCK Pulse Width High (Figure 14) | $\mathbf{5 0}$ |  | ns |


| Symbol | Parameter ( $\left.\mathrm{C}_{\mathrm{L}}=50 \mathrm{pF}\right)$ | Min | Typical (Note 10) | Max | Units |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{t}_{\mathrm{JCL}}$ | TCK Pulse Width Low (Figure 14) | 40 |  |  | ns |
| JTAG $_{\text {FMAX }}$ | TCK Maximum Frequency (Figure 14) |  |  | 10 | MHz |
| Microprocessor Interface |  |  |  |  |  |
| $\mathrm{t}_{\mathrm{csu}}$ | Control Setup before the controlling signal goes low (Figure 15) | 5 |  |  | ns |
| $\mathrm{t}_{\text {CHD }}$ | Control hold after the controlling signal goes high (Figure 15) | 5 |  |  | ns |
| $\mathrm{t}_{\text {CSPW }}$ | Controlling strobe pulse width (Write) (Figure 15) | 30 |  |  | ns |
| $\mathrm{t}_{\text {CDLY }}$ | Control output delay controlling signal low to D (Read) (Figure 15) |  |  | 30 | ns |
| $\mathrm{t}_{\mathrm{Cz}}$ | Control tri-state delay after controlling signal high (Figure 15) |  |  | 20 | ns |

Note 1: Absolute Maximum Ratings indicate limits beyond which damage to the device may occur. Operating Ratings indicate conditions for which the device is guaranteed to be functional, but do not guarantee specific performance limits. For guaranteed specifications and test conditions, see the Electrical Characteristics. The guaranteed specifications apply only for the test conditions listed. Some performance characteristics may degrade when the device is not operated under the listed test conditions. Operation of the device beyond the maximum Operating Ratings is not recommended.
Note 2: All voltages are measured with respect to GND $=A G N D=D G N D=D R G N D=0 V$, unless otherwise specified.
Note 3: When the input voltage at any pin exceeds the power supplies (that is, $\mathrm{V}_{\mathbb{I N}}<A G N D$, or $\mathrm{V}_{\mathbb{I}}>\mathrm{V}_{\mathrm{A}}$ ), the current at that pin should be limited to $\pm 25 \mathrm{~mA}$. The $\pm 50 \mathrm{~mA}$ maximum package input current rating limits the number of pins that can safely exceed the power supplies with an input current of $\pm 25 \mathrm{~mA}$ to two
Note 4: The maximum allowable power dissipation is dictated by $T_{J \text { max }}$, the junction-to-ambient thermal resistance, $\left(\theta_{J A}\right)$, and the ambient temperature, $\left(T_{A}\right)$, and can be calculated using the formula $P_{D, \max }=\left(T_{J, \max }-T_{A}\right) / \theta_{J A}$. The values for maximum power dissipation listed above will be reached only when the device is operated in a severe fault condition (e.g. when input or output pins are driven beyond the power supply voltages, or the power supply polarity is reversed). Such conditions should always be avoided.

Note 5: Human Body Model is 100 pF discharged through a $1.5 \mathrm{k} \Omega$ resistor. Machine Model is 220 pF discharged through $0 \Omega$.
Note 6: Reflow temperature profiles are different for lead-free and non-lead-free packages.
Note 7: The inputs are protected as shown below. Input voltage magnitudes above $\mathrm{V}_{\mathrm{A}}$ or below $G N D$ will not damage this device, provided current is limited per (Note 3).


Note 8: To guarantee accuracy, it is required that $\left|V_{A}-V_{D}\right| \leq 100 \mathrm{mV}$ and separate bypass capacitors are used at each power supply pin.
Note 9: With the test condition for $\mathrm{V}_{\mathrm{REF}}=+1.0 \mathrm{~V}$ ( $2 \mathrm{~V}_{\text {P-P }}$ differential input), the 12-Bit LSB is $488 \mu \mathrm{~V}$.
Note 10: Typical figures are at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ and represent most likely parametric norms at the time of product characterization. The typical specifications are not guaranteed. Test Limits are guaranteed to National's AOQL (Average Outgoing Quality Level).
Note 11: Integral Non Linearity is defined as the deviation of the analog value, expressed in LSBs, from the straight line that passes through positive and negative full-scale.
Note 12: The input capacitance is the sum of the package/pin capacitance and the sample and hold circuit capacitance.
Note 13: Timing specifications are tested at TTL logic levels, $\mathrm{V}_{\mathrm{IL}}=0.4 \mathrm{~V}$ for a falling edge and $\mathrm{V}_{\mathrm{IH}}=2.4 \mathrm{~V}$ for a rising edge.
Note 14: Optimum performance will be obtained by keeping the reference input in the 0.8 V to 1.2 V range. The LM4051CIM3-ADJ (SOT23 package) is recommended for external reference applications.
Note 15: $I_{D R}$ is the current consumed by the switching of the output drivers and is primarily determined by load capacitance on the output pins, the supply voltage, $V_{D R}$, and the rate at which the outputs are switching (which is signal dependent). $I_{D R}=V_{D R}\left(C_{0} \times f_{0}+C_{1} \times f_{1}+\ldots . C_{11} \times f_{11}\right)$ where $V_{D R}$ is the output driver power supply voltage, $\mathrm{C}_{\mathrm{n}}$ is total capacitance on the output pin, and $\mathrm{f}_{\mathrm{n}}$ is the average frequency at which that pin is toggling.
Note 16: (+x) indicates the additional dynamic range provided by the AGC. The DVGA in front of the LM97593 provides 42 dB of gain adjustment.

## DDC Timing Diagrams



FIGURE 4. LM97593 Master Reset Timing


FIGURE 5. LM97593 Synchronization Input (피) Timing


FIGURE 6. LM97593 Clock Timing


FIGURE 7. LM97593 DVGA Interface Timing


FIGURE 8. LM97593 Dual Chip Mode Timing


FIGURE 9. LM97593 Parallel Output Enable Timing


FIGURE 10. LM97593 Parallel Output Select Timing


FIGURE 11. LM97593 Parallel Output Data Ready Timing


FIGURE 12. LM97593 Debug Mode Timing


FIGURE 13. LM97593 Serial Port Timing


FIGURE 14. LM97593 JTAG Port Timing


30008716
FIGURE 15. LM97593 Control I/O Timing

## ADC Typical Performance Characteristics DNL, INL

Unless otherwise specified, the following specifications apply for AGND $=\mathrm{DGND}=\mathrm{D} 18 G N D=\mathrm{DRGND}=0 \mathrm{~V}, \mathrm{~V}_{\mathrm{A}}=\mathrm{V}_{\mathrm{D}}=\mathrm{V}_{\mathrm{DR}}=$ $+3.3 \mathrm{~V}, \mathrm{~V}_{\mathrm{D} 18}=+1.8 \mathrm{~V}, \mathrm{PD}=0 \mathrm{~V}$, Internal $\mathrm{V}_{\mathrm{REF}}=+1.0 \mathrm{~V}, \mathrm{f}_{\mathrm{CLK}}=65 \mathrm{MHz}, \mathrm{f}_{\mathrm{IN}}=12 \mathrm{MHz}, \mathrm{A}_{\mathrm{IN}}=0 \mathrm{dBFS}, \mathrm{C}_{\mathrm{L}}=10 \mathrm{pF} /$ pin, Duty Cycle Stabilizer On. Boldface limits apply for $T_{J}=T_{\text {MIN }}$ to $T_{\text {MAX }}$ : all other limits $T_{J}=25^{\circ} \mathrm{C}$

DNL


INL


## ADC Typical Performance Characteristics

Unless otherwise specified, the following specifications apply for $A G N D=D G N D=D 18 G N D=D R G N D=0 V, V_{A}=V_{D}=V_{D R}=$ $+3.3 \mathrm{~V}, \mathrm{~V}_{\mathrm{D} 18}=+1.8 \mathrm{~V}, \mathrm{PD}=0 \mathrm{~V}$, Internal $\mathrm{V}_{\mathrm{REF}}=+1.0 \mathrm{~V}, \mathrm{f}_{\mathrm{CLK}}=65 \mathrm{MHz}, \mathrm{f}_{\mathrm{IN}}=249 \mathrm{MHz}, \mathrm{A}_{\mathrm{IN}}=-9 \mathrm{dBFS}, \mathrm{C}_{\mathrm{L}}=10 \mathrm{pF} / \mathrm{pin}$, Duty Cycle Stabilizer On. Boldface limits apply for $T_{J}=T_{\text {MIN }}$ to $T_{\text {MAX }}$ : all other limits $T_{J}=25^{\circ} \mathrm{C}$

SNR, SINAD, SFDR vs. V $_{\text {SUPPLY }}$


300087102
Gain Tracking Error vs. $\mathbf{V}_{\text {SUPPLY }}$


300087104
Distortion vs. Temperature


300087106

Distortion vs. $\mathbf{V}_{\text {SUPPLY }}$


300087103
SNR, SINAD, SFDR vs. Temperature


300087105
Gain Tracking Error vs. Temperature


300087107


300087110
SNR, SINAD, SFDR vs. $\mathrm{f}_{\text {IN }}$


300087112
SNR, SINAD, SFDR vs. $\mathrm{f}_{\text {IN }}$


300087114

Distortion vs. $\mathrm{f}_{\mathrm{IN}}$
( $\mathrm{f}_{\mathrm{CLK}}=52 \mathrm{MSPS}, \mathrm{A}_{\mathrm{IN}}=-9 \mathrm{dBFS}$ )


300087111
Distortion vs. $f^{\text {N }}$
$\left(f_{\mathrm{CLK}}=52 \mathrm{MSPS}, \mathrm{A}_{\mathrm{IN}}=-3 \mathrm{dBFS}\right)$


300087113
Distortion vs. $\boldsymbol{f}_{\mathrm{IN}}$


300087115

Distortion vs. $\mathbf{f}_{\mathrm{IN}}$
( $\mathrm{f}_{\mathrm{CLK}}=65 \mathrm{MSPS}, \mathrm{A}_{\text {IN }}=-3 \mathrm{dBFS}$ )


300087116
Spectral Response @ 20MHz Input ( $\mathrm{f}_{\mathrm{CLK}}=52 \mathrm{MSPS}, \mathrm{A}_{\mathrm{IN}}=-9 \mathrm{dBFS}$ )


300087118
Spectral Response @ 20MHz Input ( $\mathrm{f}_{\mathrm{CLK}}=65 \mathrm{MSPS}, \mathrm{A}_{\mathrm{IN}}=-9 \mathrm{dBFS}$ )


300087120

Distortion vs. $\mathrm{f}_{\mathrm{IN}}$
( $\mathrm{f}_{\mathrm{CLK}}=65 \mathrm{MSPS}, \mathrm{A}_{\mathrm{IN}}=-3 \mathrm{dBFS}$ )


300087117
Spectral Response @ 20MHz Input ( $\mathrm{f}_{\mathrm{CLK}}=52 \mathrm{MSPS}, \mathrm{A}_{\mathrm{IN}}=-3 \mathrm{dBFS}$ )


300087119


300087121


IMD: $\mathrm{f}_{1 \mathrm{IN}}=246 \mathrm{MHz}, \mathrm{f}_{\text {2IN }}=250 \mathrm{MHz}$ ( $\mathrm{f}_{\mathrm{CLK}}=65 \mathrm{MSPS}, \mathrm{A}_{1 \mathrm{IN}, 21 \mathrm{~N}}=-15 \mathrm{dBFS}$ )


## CIC Output Typical Performance Characteristics

Unless otherwise specified, the following specifications apply for $A G N D=D G N D=D 18 G N D=D R G N D=0 V, V_{A}=V_{D}=V_{D R}=$ $+3.3 \mathrm{~V}, \mathrm{~V}_{\mathrm{D} 18}=+1.8 \mathrm{~V}, \mathrm{PD}=0 \mathrm{~V}$, Internal $\mathrm{V}_{\mathrm{REF}}=+1.0 \mathrm{~V}, \mathrm{f}_{\mathrm{CLK}}=65 \mathrm{MHz}, \mathrm{f}_{\mathrm{IN}}=249 \mathrm{MHz}, \mathrm{A}_{\mathrm{IN}}=-9 \mathrm{dBFS}, \mathrm{C}_{\mathrm{L}}=10 \mathrm{pF} /$ pin, Duty Cycle Stabilizer On. Boldface limits apply for $T_{J}=T_{\text {MIN }}$ to $T_{\text {MAX }}$ : all other limits $T_{J}=25^{\circ} \mathrm{C}$


300087126


300087128
Spectral Response @ 250MHz Input $\left(\mathrm{f}_{\mathrm{CLK}}=52 \mathrm{MSPS}, \mathrm{A}_{\mathrm{IN}}=-9 \mathrm{dBFS}\right)$


300087130

Spectral Response @ 20MHz Input ( $\mathrm{f}_{\mathrm{CLK}}=52 \mathrm{MSPS}, \mathrm{A}_{\mathrm{IN}}=-3 \mathrm{dBFS}$ )


300087127
Spectral Response @ 20MHz Input ( $\mathrm{f}_{\mathrm{CLK}}=65 \mathrm{MSPS}, \mathrm{A}_{\mathrm{IN}}=-3 \mathrm{dBFS}$ )


300087129
Spectral Response @ 250MHz Input ( $\mathrm{f}_{\mathrm{CLK}}=52 \mathrm{MSPS}, \mathrm{A}_{\mathrm{IN}}=-3 \mathrm{dBFS}$ )


300087131


300087132


300087133

## DDC Output Typical Performance Characteristics

Unless otherwise specified, the following specifications apply for $A G N D=D G N D=D 18 G N D=D R G N D=0 V, V_{A}=V_{D}=V_{D R}=$ $+3.3 \mathrm{~V}, \mathrm{~V}_{\mathrm{D} 18}=+1.8 \mathrm{~V}, \mathrm{PD}=0 \mathrm{~V}, \mathrm{CIC}$ decimation $=8$, Internal $\mathrm{V}_{\mathrm{REF}}=+1.0 \mathrm{~V}, \mathrm{f}_{\mathrm{CLK}}=65 \mathrm{MHz}, \mathrm{f}_{\mathrm{IN}}=249 \mathrm{MHz}, \mathrm{A}_{\text {IN }}=-9 \mathrm{dBFS}, \mathrm{C}_{\mathrm{L}}=10$ $\mathrm{pF} / \mathrm{pin}$, Duty Cycle Stabilizer On. Boldface limits apply for $\mathrm{T}_{J}=\mathrm{T}_{\text {MIN }}$ to $\mathrm{T}_{\text {MAX }}$ : all other limits $\mathrm{T}_{J}=25^{\circ} \mathrm{C}$


300087134
Spectral Response @ 20MHz Input ( $\mathrm{f}_{\mathrm{CLK}}=65 \mathrm{MSPS}, \mathrm{A}_{\mathrm{IN}}=-9 \mathrm{dBFS}$ )


300087136
Spectral Response @ 250MHz Input $\left(\mathrm{f}_{\mathrm{CLK}}=52 \mathrm{MSPS}, \mathrm{A}_{\mathrm{IN}}=-9 \mathrm{dBFS}\right)$


300087138

Spectral Response @ 20MHz Input ( $\mathrm{f}_{\mathrm{CLK}}=52 \mathrm{MSPS}, \mathrm{A}_{\mathrm{IN}}=-3 \mathrm{dBFS}$ )


300087135


300087137
Spectral Response @ 250MHz Input $\left(\mathrm{f}_{\mathrm{CLK}}=52 \mathrm{MSPS}, \mathrm{A}_{\mathrm{IN}}=-3 \mathrm{dBFS}\right)$


300087139


300087140


## Functional Description



30008717
FIGURE 16. LM97593 Dual ADC / Digital Tuner / AGC Block Diagram with Control Register Associations

The LM97593 contains two identical 12-bit ADCs driving the digital down-conversion (DDC) circuitry shown in the block diagram in Figure 16.

## ADC

The ADCs operate off of a +3.3 V supply and use a pipeline architecture with error correction circuitry to help ensure maximum performance. The differential analog input signal is digitized to 12 bits. The user has the choice of using an internal 1.0 Volt or an external reference. Any external reference is buffered on-chip to ease the task of driving that pin.
The clock frequency is rated up to 65 MHz . The analog input for both channels is acquired at the rising edge of the clock. The digital data for a given sample is delayed by the pipeline for 7 clock cycles before it reaches the input to the DDC circuit. A logic high on the power down (PD) pin reduces the converter power consumption to 50 mW . The DDC power can be further reduced by gating off the clock as described in section 7.0 Power Management.

## DDC

Each independent DDC channel down converts the sub-sampled IF to baseband, decimates the signal rate by a programmable factor ranging from 32 to 16384 , provides channel filtering, and outputs quadrature symbols.
A crossbar switch enables either of the two inputs or a test register to be routed to either DDC channel. Flexible channel filtering is provided by the two programmable decimating FIR
filters. The final filter outputs can be converted to a 12-bit floating point format or standard two's complement format. The output data is available at both serial and parallel ports. The LM97593's DDC maintains over 100 dB of spurious free dynamic range and over 100 dB of out-of-band rejection. This allows considerable latitude in channel filter partitioning between the analog and digital domains.
The frequencies, phase offsets, and phase dither of the two sine/cosine numerically controlled oscillators (NCOs) can be independently specified. Two sets of coefficient memories and a crossbar switch allow shared or independent filter coefficients and bandwidth for each channel. Both channels share the same decimation ratio and input/output formats
Each channel has its own AGC circuit for use with narrowband radio channels where most of the channel filtering precedes the ADC. The AGC closes the loop around the DVGA, compressing the dynamic range of the signal into the ADC. AGC gain compensation in the LM97593 removes the DVGA gain steps at the output. The time alignment of this gain compensation circuit can be adjusted. The AGC can be configured to operate continuously or set to a fixed gain. The two AGC circuits operate independently but share the same programmed parameters and control signals.
The chip receives configuration and control information over a microprocessor-compatible bus consisting of an 8 -bit data I/O port, an 8-bit address port, a chip enable strobe, a read strobe, and a write strobe. The chip's control registers (8 bits each) are memory mapped into the 8 -bit address space of the
control port. Page select bits allow access to the overlaid $A$ and $B$ set of FIR coefficients.
JTAG boundary scan and on-chip diagnostic circuits are provided to simplify system debug and test.
The LM97593 supports 3.3 V I/O even though the core logic voltage is 1.8 V . The LM97593 outputs swing to the 3.3 V rail so they can be directly connected to 5 V TTL inputs if desired.

## ADC Application Information

### 1.0 ADC OPERATING CONDITIONS

We recommend that the following conditions be observed for operation:

$$
\begin{aligned}
& 3.0 \mathrm{~V} \leq \mathrm{V}_{\mathrm{A}} \leq 3.6 \mathrm{~V} \\
& \mathrm{~V}_{\mathrm{D}}=\mathrm{V}_{\mathrm{A}}=\mathrm{V}_{\mathrm{DR}} \\
& \mathrm{~V}_{\mathrm{D} 18}=1.8 \mathrm{~V} \\
& 10 \mathrm{MHz} \leq \mathrm{f}_{\mathrm{CLK}} \leq 65 \mathrm{MHz} \\
& 1.0 \mathrm{~V} \text { internal reference } \\
& \mathrm{V}_{\mathrm{CM}}=1.5 \mathrm{~V} \text { (from } \mathrm{V}_{\mathrm{COM}} \mathrm{~A} \text { and } \mathrm{V}_{\mathrm{COM}} \mathrm{~B} \text { ) }
\end{aligned}
$$

### 1.1 Analog Inputs

There is one reference input pin, $\mathrm{V}_{\text {REF }}$, which is used to select an internal reference, or to supply an external reference. The ADC has two analog signal input pairs, $\mathrm{V}_{I N} \mathrm{~A}+$ and $\mathrm{V}_{I N} \mathrm{~A}$ - for one converter and $\mathrm{V}_{I N} \mathrm{~B}+$ and $\mathrm{V}_{I N} \mathrm{~B}$ - for the other converter. Each pair of pins forms a differential input pair.

### 1.2 Reference Pins

The ADC is designed to operate with an internal 1.0 V reference or an external 1.0 V reference, but performs well with external reference voltages in the range of 0.8 V to 1.2 V . Lower reference voltages will decrease the signal-to-noise ratio (SNR) of the ADC. Increasing the reference voltage (and the input signal swing) beyond 1.2 V may degrade THD for a fullscale input, especially at higher input frequencies.
It is important that all grounds associated with the reference voltage and the analog input signal make connection to the ground plane at a single, quiet point to minimize the effects of noise currents in the ground path.
The six Reference Bypass Pins ( $\mathrm{V}_{R P} \mathrm{~A}, \mathrm{~V}_{\text {COM }} \mathrm{A}, \mathrm{V}_{R N} \mathrm{~A}, \mathrm{~V}_{R P} \mathrm{~B}$, $V_{C O M} B$ and $V_{R N} B$ ) are made available for bypass purposes. All these pins should each be bypassed to ground with a 0.1 $\mu \mathrm{F}$ capacitor. A $10 \mu \mathrm{~F}$ capacitor should be placed between the $V_{R P} A$ and $V_{R N} A$ pins and between the $V_{R P} B$ and $V_{R N} B$ pins, as shown in Figure 45. This configuration is necessary to avoid reference oscillation, which could result in reduced SFDR and/or SNR.
Smaller capacitor values than those specified will allow faster recovery from the power down mode, but may result in degraded noise performance. Loading any of these pins other than $\mathrm{V}_{\text {Сом }} \mathrm{A}$ and $\mathrm{V}_{\text {Сом }} \mathrm{B}$ may result in performance degradation.
The nominal voltages for the reference bypass pins are as follows:

$$
\begin{aligned}
& \mathrm{V}_{\mathrm{COM}}=1.5 \mathrm{~V} \\
& \mathrm{~V}_{\mathrm{RP}}=\mathrm{V}_{\mathrm{COM}}+\mathrm{V}_{\mathrm{REF}} / 2 \\
& \mathrm{~V}_{\mathrm{RN}}=\mathrm{V}_{\mathrm{COM}}-\mathrm{V}_{\mathrm{REF}} / 2
\end{aligned}
$$

User choice of an on-chip or external reference voltage is provided. The internal 1.0 Volt reference is in use when the the $\mathrm{V}_{\text {REF }}$ pin is connected to $\mathrm{V}_{\mathrm{A}}$. If a voltage in the range of 0.8 V to 1.2 V is applied to the $\mathrm{V}_{\text {REF }}$ pin, that is used for the voltage reference. When an external reference is used, the $\mathrm{V}_{\text {REF }}$ pin should be bypassed to ground with a $0.1 \mu \mathrm{~F}$ capacitor
close to the reference input pin. There is no need to bypass the $V_{\text {REF }}$ pin when the internal reference is used.

### 1.3 Signal Inputs

The signal inputs are $\mathrm{V}_{\text {IN }} A+$ and $\mathrm{V}_{\text {IN }} A$ - for one $A D C$ and $V_{I N} B+$ and $V_{I N} B$ - for the other $A D C$. The input signal, $V_{\mathbb{I N}}$, is defined as

$$
\begin{equation*}
V_{I N} A=\left(V_{I N} A+\right)-\left(V_{I N} A-\right) \tag{Eq.1}
\end{equation*}
$$

for the "A" converter and

$$
\begin{equation*}
V_{I N} B=\left(V_{I N} B+\right)-\left(V_{I N} B-\right) \tag{Eq.2}
\end{equation*}
$$

for the " B " converter. Figure 17 shows the expected input signal range. Note that the common mode input voltage, $\mathrm{V}_{\mathrm{CM}}$, should be in the range of 1.0 V to 2.0 V .
The peaks of the individual input signals should never exceed 2.6 V .

The ADC performs best with a differential input signal with each input centered around a common mode voltage, $\mathrm{V}_{\mathrm{CM}}$. The peak-to-peak voltage swing at each analog input pin should not exceed the value of the reference voltage or the output data will be clipped.
The two input signals should be exactly $180^{\circ}$ out of phase from each other and of the same amplitude. For single frequency inputs, angular errors result in a reduction of the effective full scale input. For complex waveforms, however, angular errors will result in distortion.

(a) Differential Input

(b) Single-Ended Input

30008750

## FIGURE 17. Expected Input Signal Range

For single frequency sine waves the full scale error in LSBs can be described as approximately
$\mathrm{E}_{\mathrm{FS}}=4096\left(1-\sin \left(90^{\circ}+\mathrm{dev}\right)\right)$
Where dev is the angular difference in degrees between the two signals having a $180^{\circ}$ relative phase relationship to each other (see Figure 18). Drive the analog inputs with a source impedance less than $100 \Omega$.


30008751
FIGURE 18. Angular Errors Between the Two Input Signals Will Reduce the Output Level or Cause Distortion

For differential operation, each analog input pin of the differential pair should have a peak-to-peak voltage equal to the
reference voltage, $\mathrm{V}_{\mathrm{REF}}$, be 180 degrees out of phase with each other and be centered around $\mathrm{V}_{\mathrm{CM}}$.

### 1.3.1 Single-Ended Operation

Performance with differential input signals is better than with single-ended signals. For this reason, single-ended operation is not recommended. However, if single ended-operation is required and the resulting performance degradation is acceptable, one of the analog inputs should be connected to the d.c. mid point voltage of the driven input. The peak-to-peak input signal at the driven input pin should be twice the reference voltage to maximize SNR and SINAD performance (Figure 17 b ). For example, set $\mathrm{V}_{\mathrm{REF}}$ to 1.0 V , bias $\mathrm{V}_{\mathrm{IN}^{-}}$to 1.5 V and drive $\mathrm{V}_{\mathrm{IN}^{+}}+$with a signal range of 0.5 V to 2.5 V .
Because very large input signal swings can degrade distortion performance, better performance with a single-ended input can be obtained by reducing the reference voltage when maintaining a full-range output.

### 1.3.2 Driving the Analog Inputs

The $\mathrm{V}_{\mathrm{IN}^{+}}$and the $\mathrm{V}_{\mathrm{IN}^{-}}$inputs of the ADC consist of an analog switch followed by a switched-capacitor amplifier. As the internal sampling switch opens and closes, current pulses occur at the analog input pins, resulting in voltage spikes at the signal input pins. As the driving source attempts to counteract these voltage spikes, it may add noise to the signal at the ADC analog input. C1, C2, and C3 as shown in Figure 45 improve the ADC performance by filtering these voltage spikes. These components should be placed close to the ADC inputs because the input pins of the ADC are the most sensitive part of the system and this is the last opportunity to filter that input.
For Nyquist applications the RC pole should be at the ADC sample rate. The ADC input capacitance in the sample mode should be considered when setting the RC pole. For wideband undersampling applications, the RC pole should be set at about 1.5 to 2 times the maximum input frequency to maintain a linear delay response. The values of the RC shown in Figure 45 are suitable for applications with input frequencies up to approximately 70 MHz .

### 1.3.3 Input Common Mode Voltage

The input common mode voltage, $\mathrm{V}_{\mathrm{CM}}$, should be in the range of 1.0 V to 2.0 V and be a value such that the peak excursions of the analog signal do not go more negative than ground or more positive than 2.6V. See Section 1.2.

### 2.0 DIGITAL INPUTS

Digital TTL/CMOS compatible inputs consist of CK, REFSEL/ DCS.

### 2.1 CLK

The CLK signal controls the timing of the sampling process. Drive the clock input with a stable, low jitter clock signal in the range of 10 MHz to 65 MHz . The higher the input frequency, the more critical it is to have a low jitter clock. The trace carrying the clock signal should be as short as possible and should not cross any other signal line, analog or digital, not even at $90^{\circ}$.
The CLK signal also drives an internal state machine. If the CLK is interrupted, or its frequency too low, the charge on internal capacitors can dissipate to the point where the accuracy of the output data will degrade. This is what limits the lowest sample rate.
The clock line should be terminated at its source in the characteristic impedance of that line. Take care to maintain a constant clock line impedance throughout the length of the
line. Refer to Application Note AN-905 for information on setting characteristic impedance.
It is highly desirable that the the source driving the ADC CLK pin only drive that pin. However, if that source is used to drive other things, each driven pin should be a.c. terminated with a series RC to ground such that the resistor value is equal to the characteristic impedance of the clock line and the capacitor value is

$$
\begin{equation*}
C \geq \frac{4 \times t_{P D} \times L}{Z_{o}} \tag{Eq.4}
\end{equation*}
$$

where $t_{P D}$ is the signal propagation time down the clock line, " $L$ " is the line length and $Z_{O}$ is the characteristic impedance of the clock line. This termination should be as close as possible to the ADC clock pin but beyond it as seen from the clock source. Typical $t_{P D}$ is about $150 \mathrm{ps} / \mathrm{inch}(60 \mathrm{ps} / \mathrm{cm})$ on FR-4 board material. The units of "L" and $t_{P D}$ should be the same (inches or centimeters).
The duty cycle of the clock signal can affect the performance of the A/D Converter. Because achieving a precise duty cycle is difficult, the LM97593 has a Duty Cycle Stabilizer which can be enabled using the REFSEL/DCS pin. It is designed to maintain performance over a clock duty cycle range of $30 \%$ to $70 \%$ at 65 MSPS .

### 2.2 REFSEL/DCS

This pin is used in conjunction with $\mathrm{V}_{\text {REF }}$ (pin 21) to select the reference source and turn the Duty Cycle Stabilizer (DCS) on or off.
When REFSEL/DCS is LOW and $\mathrm{V}_{\text {REF }}$ is HIGH, the internal 1.0 V reference is selected and DCS is On.

When REFSEL/DCS is HIGH, an external reference voltage in the range of 0.8 V to 1.2 V should be applied to the VREF input. DCS is On.
With REFSEL/DCS pin connected to $\mathrm{V}_{\text {COM }} \mathrm{A}$ or $\mathrm{V}_{\text {COM }} \mathrm{B}$, the internal 1.0V reference is selected and DCS is Off.
When enabled, duty cycle stabilization can compensate for clock inputs with duty cycles ranging from $30 \%$ to $70 \%$ and generate a stable internal clock, improving the performance of the part.

TABLE 1. $\mathrm{V}_{\text {REF }}$, REFSEL/DCS Pin Functions

| REFSEL/ <br> DCS (pin 8) | $\mathbf{V}_{\text {REF }}$ (pin 21) | Reference | DCS |
| :--- | :--- | :--- | :--- |
| Logic Low | Logic High | Internal 1.0 V | ON |
| Logic High | 0.8 to 1.2V | External | ON |
| $\mathrm{V}_{\text {COM }}$ A or <br> $\mathrm{V}_{\text {COM }} \mathrm{B}$ | Logic High | Internal 1.0V | OFF |
| $\mathrm{V}_{\text {COM }} \mathrm{A}$ or <br> $\mathrm{V}_{\mathrm{COM}} \mathrm{B}$ | 0.8 to 1.2V | External | OFF |

### 2.3 PD

The PD pin, when high, holds the ADC in a power-down mode to conserve power when the converter is not being used. The output data pins are undefined and the data in the pipeline is corrupted while in the power down mode.
The Power Down Mode Exit Cycle time is determined by the value of the components on pins $15,16,17,22,23$ and 24. These capacitors lose their charge in the Power Down mode and must be recharged by on-chip circuitry before conversions can be accurate. Smaller capacitor values allow slightly faster recovery from the power down mode, but can result in a reduction in SNR, SINAD and ENOB performance.

## DDC Application Information

### 3.0 CONTROL INTERFACE

The LM97593 is configured by writing control information into 237 control registers within the chip. The contents of these control registers and how to use them are described in section 9.1 Control Register Addresses and Defaults. The registers are written to or read from using the D[7:0], A[7:0], CE, RD and WR pins. This interface is designed to allow the LM97593 to appear to an external processor as a memory mapped peripheral. See Figure 15 for details.
The control interface is asynchronous with respect to the system clock, CK. This allows the registers to be written or read at any time. In some cases this might cause an invalid operation since the interface is not internally synchronized. In order to assure correct operation, $\overline{\mathbf{S I}}$ must be asserted after the control registers are written.
The D[7:0], A[7:0], $\overline{\mathbf{W R}}, \overline{\mathrm{RD}}$ and $\overline{\mathbf{C E}}$ pins should not be driven above the positive supply voltage.

### 3.1 Master Reset

A master reset pin, $\overline{\mathbf{M R}}$, is provided to initialize the LM97593 to a known condition and should be strobed after power up. This signal will clear all sample data and all user programmed data (filter coefficients and AGC settings). All outputs will be disabled (tri-stated). $\overline{\text { ASTROBE }}$ and BSTROBE will be asserted to initialize the DVGA values. Section 9.1 Control Register Addresses and Defaults describes the control register default values.

### 3.2 Synchronizing Multiple LM97593 Chips

A system containing two or more LM97593 chips will need to be synchronized if coherent operation is desired. To synchronize multiple LM97593 chips, connect all of the sync input pins together so they can be driven by a common sync strobe. Synchronization occurs on the first rising edge of CK after $\mathbf{S I}$ goes high. When $\overline{\mathbf{S I}}$ is asserted all sample data is immediately cleared, the numerically controlled oscillator (NCO) phase offset is initialized, the NCO dither generators are reset, and the CIC decimation ratio is initialized. Only the configuration data loaded into the microprocessor interface remains unaffected.
SI may be held low as long as desired after a minimum of 4 CK periods.

### 3.3 Input Source

The input crossbar switch allows either $\mathbf{V}_{\text {IN }} \mathbf{A}, \mathbf{V}_{\text {IN }} \mathbf{B}$, or a test register to be routed to the channel A or channel B AGC/ DDC. The AGC outputs, AGAIN and BGAIN, are not switched. If $V_{I N} A$ and $V_{I N} B$ are exchanged the AGC loop will be open and the $A G C$ will not function properly.
Selecting the test register as the input source allows the AGC or DDC operation to be verified with a known input. See section 8.0 Test and Diagnostics for further discussion.

### 4.0 DOWN CONVERTERS

A detailed block diagram of each DDC channel is shown in Figure 19. Each down converter uses a complex NCO and mixer to quadrature downconvert a signal to baseband. The "FLOAT TO FIXED CONVERTER" treats the 15-bit mixer output as a mantissa and the AGC output, EXP, as a 3-bit exponent. It performs a bit shift on the data based on the value of EXP. This bit shifting is used to expand the compressed dynamic range resulting from the DVGA operation. The DVGA gain is adjusted in 6dB steps which are equivalent to each digital bit shift.
Digitally compensating for the DVGA gain steps in the LM97593 causes the DDC output to be linear with respect to the DVGA input. The AGC operation will be completely transparent at the LM97593 output.
The exponent (EXP) can be forced to its maximum value by setting the EXP_INH bit. If $x_{\text {in }}(n)$ is the DDC input, the signal after the "FLOAT TO FIXED CONVERTER" is

$$
x_{3}(n)=x_{i n}(n)^{*} \cos (\omega n)^{*} 2 \operatorname{ExP}
$$

for the I component. Changing the 'cos' to 'sin' in this equation will provide the Q component.
The "FLOAT TO FIXED CONVERTER" circuit expands the dynamic range compression performed by the DVGA. Signals from this point onward extend across the full dynamic range of the signals applied to the DVGA input. This allows the AGC to operate continuously through a burst without producing artifacts in the signal due to the settling response of the decimation filters after a 6dB DVGA gain adjustment. For example, if the DVGA input signal were to increase causing the ADC output level to cross the AGC threshold level, the gain of the DVGA would change by -6 dB . The 6 dB step is allowed to propagate through the ADC and mixers and is compensated out just before the filtering. The accuracy of


FIGURE 19. LM97593 Down Converter, Channel A (Channel B is identical)
the compensation is dependent on timing and the accuracy of the DVGA gain step. The LM97593 allows the timing of the gain compensation to be adjusted in the EXT_DELAY register; see the end of section 6.0 AGC for more information. The AGC requires 21 bits (14-bit internal bus output + 7-bit shift) to represent the full linear dynamic range of the signal. The output word must be set to either 24-bit or 32-bit to take advantage of the entire dynamic range available. The LM97593 can also be configured to output a floating point format with up to 138 dB of numerical resolution using only 12 output bits. The "SHIFT UP" circuit will be discussed in the section 4.2 Four Stage CIC Filter.
A 4-stage cascaded-integrator-comb (CIC) filter and a twostage decimate by 4 or 8 finite impulse response (FIR) filter are used to lowpass filter and isolate the desired signal. The CIC filter reduces the sample rate by a programmable factor ranging from 8 to 2048 (decimation ratio). The CIC outputs are followed by a gain stage and then followed by a two-stage decimate by 4 or 8 filter. The gain circuit allows the user to boost the gain of weak signals by up to 42 dB in 6 dB steps. It also rounds the signal to 21 bits and saturates at plus or minus full scale.
The first stage of the two stage filter is a 21-tap, symmetric decimate by 2 FIR filter (F1) with programmable 16 bit tap weights. The coefficients of the first 11 taps are downloaded to the chip as 16 bit words. Since the filter is a symmetric configuration only the first 11 coefficients must be loaded. Section 4.4 First Programmable FIR Filter provides a generic set of coefficients that compensate for the rolloff of the CIC filter and provide a passband flat to 0.01 dB with 70 dB of out of band rejection. A second coefficient set is provided that has a narrower output passband and greater out-of-band rejection. The second set of coefficients is ideal for systems such as GSM where far-image rejection is more important than adjacent channel rejection.
The second stage is a 63 tap decimate by 2 or 4 programmable FIR filter (F2) also with 16 bit tap weights. Filter coefficients for a flat response from -0.4 FS to +0.4 FS of the


FIGURE 20. Example of NCO spurs due to phase truncation (Before Phase Dithering)
output sample rate with 80 dB of out of band rejection are provided in Section 4.5 Second Programmable FIR Filter. A second set of F 2 coefficients is also provided to enhance per-
formance for GSM systems. The user can also design and download their own final filter to customize the channel's spectral response. Typical uses of programmable filter F2 include matched (root-raised cosine) filtering, or filtering to generate oversampled outputs with greater out of band rejection. The 63 tap symmetrical filter is downloaded into the chip as 32 words, 16 bits each. Saturation to plus or minus full scale is performed at the output of F1 and F2 to clip the signal rather than allow it to roll over.
The LM97593 provides two sets of coefficient memory for both F1 and F2. These coefficient memories can be independently routed to channel A, channel B, or both channel A and $B$ with a crossbar switch. The coefficients can be switched on the fly but some time will be required before valid output data is available.

### 4.1 The Numerically Controlled Oscillator

The tuning frequency of each down converter is specified as a 32 bit word ( .02 Hz resolution at $\mathbf{C K}=52 \mathrm{MHz}$ ) and the phase offset is specified as a 16 bit word (.0050). These two parameters are applied to the Numerically Controlled Oscillator (NCO) circuit to generate sine and cosine signals used by the digital mixer. The NCOs can be synchronized with NCOs on other chips via the sync pin $\overline{\mathbf{S}}$. This allows multiple down converter outputs to be coherently combined, each with a unique phase and amplitude.
The tuning frequency is set by loading the FREQ register according to the formula $\mathrm{FREQ}=2^{32} \mathrm{~F} / \mathrm{F}_{\mathrm{CK}}$, where F is the desired tuning frequency and $\mathrm{F}_{\mathrm{CK}}$ is the chip's clock rate. FREQ is a 2's complement word. The range for $F$ is from $-F C K / 2$ to + FCK $\left(1-2^{-31}\right) / 2$.
If a sub-sampled signal is in an even Nyquist zone the sampling process causes the order of the I and Q components to be reversed. Should this occur simply invert the polarity of the tuning frequency $F$.


30008799
FIGURE 21. Example of NCO spurs due to phase truncation
(After Phase Dithering)
The 2's complement format represents full-scale negative as 10000000 and full-scale positive as 01111111 for an 8 -bit example.
The 16 bit phase offset is set by loading the PHASE register according to the formula PHASE $=2^{16} P / 2 \pi$, where $P$ is the desired phase in radians ranging between 0 and $2 \pi$. PHASE
is an unsigned 16 -bit number. P ranges from 0 to $2 \pi\left(1-2^{-16}\right)$. Phase dithering can be enabled to reduce the spurious signals created by the NCO due to phase truncation. This truncation is unavoidable since the frequency resolution is much finer than the phase resolution. With dither enabled, spurs due to phase truncation are below -100 dBc for all frequencies and phase offsets. Each NCO has its own dither source and the initial state of one is maximally offset with respect to the other so that they are effectively uncorrelated. The phase dither sources are on by default. They are independently controlled by the DITH_A and DITH_B bits. The amplitude resolution of the ROM creates a worst-case spur amplitude of -101 dBc rendering amplitude dither unnecessary.
The spectrum plots in Figure 20 and Figure 21show the effectiveness of phase dither in reducing NCO spurs due to phase truncation for a worst-case example (just below $F_{S} / 8$ ). With dither off, the spur is at -86.4 dBFS . With dither on, the spur is below -125 dBFS , disappearing into the noise floor. This spur is spread into the noise floor which results in an SNR of -83.6dBFS. The channel filter's processing gain will further improve the SNR.
Figure 22 shows the spur levels as the tuning frequency is scanned over a narrow portion of the frequency range. The spurs are again a result of phase quantization but their locations move about as the frequency scan progresses. As before, the peak spur level drops when dithering is enabled. When dither is enabled and the fundamental frequency is exactly at $\mathrm{F}_{\mathrm{S}} / 8$, the worst-case spur due to amplitude quantization can be observed at -101dBc in Figure 23.

### 4.2 Four Stage CIC Filter

The mixer outputs are decimated by a factor of N in a four stage CIC filter. N is programmable to any integer between 8 and 2048. Decimation is programmed in the DEC register where $D E C=\mathrm{N}-1$. The programmable decimation allows the chip's usable output bandwidth to range from about $\pm 1.27 \mathrm{kHz}$ to $\pm 650 \mathrm{kHz}$ when the input data rate (which is equal to the chip's clock rate, $\mathrm{F}_{\mathrm{CK}}$ ) is 52 MHz . For the maximum sample rate of 65 MHz , the LM97593's output bandwidth will range from about $\pm 1.58 \mathrm{kHz}$ to $\pm 812 \mathrm{kHz}$. A block diagram of the CIC filter is shown in Figure 24.
The CIC filter is primarily used to decimate the high-rate incoming data while providing a rough lowpass characteristic. The lowpass filter will have a $\sin (x) / x$ response (similar to the AGC's CIC shown in Figure 39) where the first null is at $\mathrm{F}_{\mathrm{S}} / \mathrm{N}$.


30008720
FIGURE 22. NCO Spurs due to Phase Quantization


30008721
FIGURE 23. Worst Case Amplitude Spur, NCO at $\mathrm{F}_{\mathbf{S}} / 8$
The CIC filter has a gain equal to $\mathrm{N}^{4}$ (filter decimation^4) which must be compensated for in the "SHIFT UP" circuit shown in Figure 24 as well as Figure 19. This circuit has a gain equal to 2 (SCALE-44), where SCALE ranges from 0 to 40 . This circuit divides the input signal by $2^{44}$ providing


30008722
FIGURE 24. Four-stage decimate by N CIC filter
maximum headroom through the CIC filter. For optimal noise performance the SCALE value is set to increase this level until
the CIC filter is just below the point of distortion. A value is normally calculated and loaded for SCALE such that

GAIN $N_{\text {SHIFTUP }}{ }^{*} G A I N_{C I C} \leq 1$. The actual gain of the CIC filter will only be unity for power-of-two decimation values. In other cases the gain will be somewhat less than unity.

### 4.3 Channel Gain

The gain of each channel can be boosted up to 42 dB by shifting the output of the CIC filter left by 0 to 7 bits prior to rounding it to 21 bits. For channel $A$, the gain of this stage is: GAIN $=2$ GAIN_A , where GAIN_A ranges from 0 to 7 . Overflow due to the GAIN circuit is saturated (clipped) at plus or minus full scale. Each channel can be given its own GAIN setting.

### 4.4 First Programmable FIR Filter (F1)

The CIC/GAIN outputs are followed by two stages of filtering. The first stage is a 21 tap decimate-by-2 symmetric FIR filter with programmable coefficients. Typically, this filter compensates for a slight droop induced by the CIC filter while removing undesired alias images above Nyquist. In addition, it often provides stopband assistance to F2 when deep stop bands are required. The filter coefficients are 16-bit 2's complement numbers. Unity gain will be achieved through the filter if the sum of the 21 coefficients is equal to $2^{16}$. If the sum is not $2^{16}$, then $F 1$ will introduce a gain equal to (sum of coefficients)/ $2^{16}$. The 21 coefficients are identified as coefficients $h_{1}(n), \mathrm{n}$ $=0, \ldots, 20$ where $h_{1}(10)$ is the center tap. The coefficients are symmetric, so only the first 11 are loaded into the chip.
Two example sets of coefficients are provided here. The first set of coefficients, referred to as the standard set (STD), compensates for the droop of the CIC filter providing a passband which is flat ( 0.01 dB ripple) over $95 \%$ of the final output bandwidth with 70 dB of out-of-band rejection (see Figure 25). The filter has a gain of 0.999 and is symmetric with the following 11 unique taps ( $1|21,2| 20, \ldots, 10 \mid 12,11$ ):

$$
29,-85,-308,-56,1068,1405,-2056,-6009,
$$ 1303, 21121, 32703



FIGURE 25. F1 STD frequency response
The second set of coefficients (GSM set) are intended for applications that need deeper stop bands or need oversampled outputs. These requirements are common in cellular systems where out of band rejection requirements can exceed 100 dB (see Figure 26). They are useful for wideband radio architectures where the channelization is done after the ADC. These filter coefficients introduce a gain of 0.984 and are:

$$
\begin{aligned}
& -49,-340,-1008,-1617,-1269,425,3027,6030 \\
& 9115,11620,12606
\end{aligned}
$$



FIGURE 26. F1 GSM frequency response

### 4.5 Second Programmable FIR Filter (F2)

The second stage decimate by two or four filter also uses externally downloaded filter coefficients. F2 determines the final channel filter response. The filter coefficients are 16-bit 2's complement numbers. Unity gain will be achieved through the filter if the sum of the 63 coefficients is equal to $2^{16}$. If the sum is not $2^{16}$, then the F2 will introduce a gain equal to (sum of coefficients)/2 ${ }^{16}$.
The 63 coefficients are identified as $h_{2}(n), n=0, \ldots, 62$ where $h_{2}(31)$ is the center tap. The coefficients are symmetric, so only the first 32 are loaded into the chip. An example filter (STD F2 coefficients, see Figure 27) with 80dB out-of-band rejection, gain of 1.00 , and 0.03 dB peak to peak passband ripple is created by this set of 32 unique coefficients:

$$
\begin{aligned}
& -14,-20,19,73,43,-70,-82,84,171,-49,-269, \\
& -34,374,192,-449, \\
& -430,460,751,-357,-1144,81,1581,443,-2026, \\
& -1337,2437,2886, \\
& -2770,-6127,2987,20544,29647
\end{aligned}
$$

A second set of F2 coefficients (GSM set, see Figure 28) suitable for meeting the stringent wideband GSM requirements with a gain of 0.999 are:

$$
\begin{aligned}
& -536,-986,42,962,869,225,141,93,-280, \\
& -708,-774,-579,-384, \\
& -79,536,1056,1152,1067,789,32,-935,-1668, \\
& -2104,-2137,-1444, \\
& 71,2130,4450,6884,9053,10413,10832
\end{aligned}
$$

The filter coefficients of both filters can be used to tailor the spectral response to the user's needs. For example, the first can be loaded with the standard set to provide a flat


30008725
FIGURE 27. F2 STD frequency response


30008726

## FIGURE 28. F2 GSM frequency response

response through to the second filter. The latter can then be programmed as a Nyquist (typically a root-raised-cosine) filter for matched filtering of digital data.
The complete channel filter response for standard coefficients is shown in Figure 29. Passband flatness is shown in Figure 30. The complete filter response for GSM coefficients is shown in Figure 31. GSM Passband flatness is shown in Figure 32.
The mask shown in Figure 31 is derived from the ETSI GSM 5.05 specifications for a normal Basestation Transceiver (BTS). For interferers, 9 dB was added to the carrier to interference ( $\mathrm{C} / \mathrm{I}$ ) ratios. For blockers, 9 dB was added to the difference between the blocker level and 3dB above the reference sensitivity level.

### 4.6 Channel Bandwidth vs. Sample Rate

When the LM97593 is used for GSM systems, a bandwidth of about 200 kHz is desired. With a sample rate of 52 MHz , the total decimation of 192 provides the desired 270.833 kHz output sample rate. This output sample rate in combination with the FIR filter coefficients create the desired channel bandwidth. If the sample rate is increased to 65 MHz , the decimation must also be increased to $65 \mathrm{MHz} / 270.833 \mathrm{kHz}$ or 240 . This new decimation rate will maintain the same output


30008727
FIGURE 29. CIC, F1, \& F2 STD frequency response


FIGURE 30. CIC, F1, \& F2 STD Passband Flatness


FIGURE 31. CIC, F1, \& F2 GSM frequency response
bandwidth. The output bandwidth may only be changed in relation to the output sample rate by creating a new set of FIR filter coefficients. As the filter bandwidth


FIGURE 32. CIC, F1, \& F2 GSM Passband Flatness
decreases relative to the output sample rate, the CIC droop compensation performed by F1 may no longer be required.

### 4.7 Overall Channel Gain

The overall gain of the chip is a function of the amount of decimation ( N ), the settings of the "SHIFT UP" circuit (SCALE), the GAIN setting, the sum of the F1 coefficients, and the sum of the F2 coefficients. The overall gain is shown below in Equation 2.

$$
\begin{align*}
G_{D D C}= & \frac{1}{2}(D E C+1)^{4} \\
& \cdot 2^{\left[S C A L E-44-A G A I N \cdot\left(1-E X P_{-} I N I I\right)\right]}  \tag{Eq.6}\\
& \cdot 2^{\text {CAIN }} \\
& \cdot G_{F 1} \cdot G_{F 2}
\end{align*}
$$

Where:

$$
\begin{equation*}
G_{l, 1}=\frac{\sum_{i=1}^{21} h_{1}(i)}{2^{16}} \tag{Eq.7}
\end{equation*}
$$

and:

$$
\begin{equation*}
G_{F 2}=\frac{\sum_{i=1}^{63} h_{2}(i)}{2^{16}} \tag{Eq.8}
\end{equation*}
$$

It is assumed that the DDC output words are treated as fractional 2's complement words. The numerators of $G_{F 1}$ and $G_{F 2}$ equal the sums of the impulse response coefficients of F1 and F2, respectively. For the STD and GSM sets, $G_{F 1}$ and $\mathrm{G}_{\mathrm{F} 2}$ are nearly equal to unity. Observe that the AGAIN term in (Eq. 6) is cancelled by the DVGA operation so that the entire gain of the DRCS is independent of the DVGA setting when EXP_INH=0. The $1 / 2$ appearing in (Eq. 6) is the result of the 6 dB conversion loss in the mixer. For full-scale square
wave inputs the $1 / 2$ should be set to 1 to prevent signal distortion.

### 4.8 Data Latency and Group Delay

The LM97593 latency calculation assumes that the FIR filter latency will be equal to the time required for data to propagate through one half of the taps. The CIC filter provides 4 N equivalent taps where N is the CIC decimation ratio. F 1 and F 2 provide 21 and 63 taps respectively. When these filters are reflected back to the input rate, the effective taps are increased by decimation. This results in a total of 151 N taps.
The total latency is found by dividing the number of taps by 2 and adding pipeline delays. When the F2 decimation is 2 the latency is 80 N . When the F2 decimation is 4 the latency is 82N. The LM97593 filters are linear phase filters so the group delay remains constant.

### 5.0 OUTPUT MODES

After processing by the DDC, the data is then formatted for output.
All output data is two's complement. The serial outputs power up in a tri-state condition and must be enabled when the chip is configured. Parallel outputs are enabled by the POUT_EN pin.
Output formats include truncation to 8 or 32 bits, rounding to 16 or 24 bits, and a 12-bit floating point format (4-bit exponent, 8 -bit mantissa, 138 dB numeric range). This function is performed in the OUTPUT CIRCUIT shown in Figure 33.


30008731
FIGURE 33. LM97593 output circuit
The channel outputs are accessible through serial output pins and a 16-bit parallel output port. The RDY pin is provided to notify the user that a new output sample period (OSP) has begun. OSP refers to the interval between output samples at the decimated output rate. For example, if the input rate (and clock rate) is 52 MHz and the overall decimation factor is 192 ( $\mathrm{N}=48$, F 2 decimation $=2$ ) the OSP will be 3.69 microseconds which corresponds to an output sample


FIGURE 34. Serial output formats. Refer to Figure 13 for detailed timing information
rate of 270.833 kHz . An OSP starts when a sample is ready and stops when the next one is ready.

### 5.1 Serial Outputs

The LM97593 provides a serial clock (SCK), a frame strobe (SFS) and two data lines (AOUT and BOUT) to output serial data. The MUX_MODE control register specifies whether the two channel outputs are transmitted on two separate serial pins, or multiplexed onto one pin in a time division multiplexed (TDM) format. Separate output pins are not provided for the I and $Q$ halves of complex data. The I and Q outputs are always multiplexed onto the same serial pin. The I-component is output first, followed by the Q-component. By setting the PACKED mode bit to ' 1 ' a complex pair may be treated as a single double-wide word. The RDY signal is used to identify the first word of a complex pair of the TDM formatted output when the SFS_MODE bit is set to ' 0 '. Setting SFS_MODE to ' 1 ' causes the LM97593 to output a single SFS pulse for each
output period. This SFS pulse will be coincident with RDY and only a single SCK period wide. The TDM modes are summarized in Table 2.

TABLE 2. TDM Modes

| SFS_MODE | MUX_MODE | SERIAL OUTPUTS |  |
| :---: | :---: | :---: | :---: |
|  |  | AOUT | BOUT |
| 0 | 0 | $\mathrm{OUT}_{\mathrm{A}}$ | $\mathrm{OUT}_{\text {B }}$ |
|  | 1 | $\mathrm{OUT}_{\mathrm{A}}, \mathrm{OUT}_{\mathrm{B}}$ | LOW |
| 1 | 0 | $\mathrm{OUT}_{\mathrm{A}}$ | $\mathrm{OUT}_{\mathrm{B}}$ |
|  | 1 | $\mathrm{OUT}_{\mathrm{A}}, \mathrm{OUT}_{\mathrm{B}}$ | LOW |

The serial outputs use the format shown in Figure 34. Figure 34(a) shows the standard output mode (the PACKED mode bit is low). The chip clocks the frame and data out of the chip


## FIGURE 35. Serial Daisy-Chain Mode

on the rising edge of SCK (or falling edge if the SCK_POL bit in the input control register is set high). Data should be captured on the falling edge of SCK (rising if SCK_POL=1). The chip sends the I data first by setting SFS high (or low if SFS_POL in the input control register is set high) for one clock cycle, and then transmitting the data, MSB first, on as many SCK cycles as are necessary. Without a pause, the $Q$ data is transferred next as shown in Figure 34(a). If the PACKED control bit is high, then the I and Q components are sent as a double length word with only one SFS strobe as shown in Figure 34(b). If both channels are multiplexed out the same serial pin, then the subsequent I/Q channel words will be transmitted immediately following the first I/Q pair as shown in Figure 34(c). Figure 34(c) also shows how SFS_MODE=1 allows the SFS signal to be used to identify the A and B channels in the TDM serial transmission. The serial output rate is programmed by the RATE register to CK divided by 1, 2, 4, 8,16 , or 32 . The serial interface will not work properly if the programmed rate of SCK is insufficient to clock out all the bits in one OSP.

### 5.2 Serial Port Daisy-Chain Mode

Two LM97593s can be connected in series so that a single DSP serial port can receive four DDC output channels. This mode is enabled by setting the SDC_EN bit to ' 1 ' ' on the serial daisy-chan (SDC) master. The SDC master is the LM97593 which is connected to the DSP while the SDC slave's serial output drives the master. The SDC master's RATE register must be set so that its SCK rate is twice that of the SDC slave, the SDC master must have MUX_MODE=1, the SDC slave must have MUX_MODE=0 and PACKED=1, and both chips must come out of a MR or SI event within four CK periods of each other. In this configuration, the master's serial output data is shifted out to the DSP and then the slave's serial data is shifted out. All the serial output data will be muxed onto the master's AOUT pin as shown in Figure 35.

### 5.3 Serial Port Output Number Formats

Several numeric formats are selectable using the FORMAT control register. The I/Q samples can be rounded to 16 or 24 bits, or truncated to 8 bits. The packed mode works as described above for these fixed point formats. A floating point format with 138 dB of dynamic range in 12 bits is also provided. The mantissa ( m ) is 8 bits and the exponent (e) is 4 bits. The MSB of each segment is transmitted first. When the packed mode is selected, the I/Q samples are packed re-
gardless of the state of MUX_MODE, and the data is sent as $\mathrm{ml} / \mathrm{el} / \mathrm{eQ} / \mathrm{mQ}$ which allows the two exponents to form an 8bit word. This is shown in Figure 34(d). For all formats, once the defined length of the word is complete, SCK stops toggling.

### 5.4 Parallel Outputs

Output data from the channels can also be taken from a 16bit parallel port. A 3-bit word applied to the POUT_SEL[2:0] pins determines which 16-bit segment is multiplexed to the parallel port. Table 3 defines this mapping. To allow for bussing of multiple chips, the parallel port is tri-stated unless $\overline{\text { POUT_EN }}$ is low. The RDY signal indicates the start of an OSP and that new data is ready at the parallel output. The user has one OSP to cycle through whichever registers are needed. The RATE register must be set so that each OSP is at least 5 SCK periods.

### 5.4.1 Parallel Port Output Numeric Formats

The I/Q samples can be rounded to 16 or 24 bits or the full 32 bit word can be read. By setting the word size to 32 bits it is possible to read out the top 16 -bits and only observe the top 8 bits if desired. Additionally, the output samples can be formatted as floating point numbers with an 8-bit mantissa and a 4 bit exponent. For the fixed-point formats, the valid bits are justified into the MSBs of the registers of Table 3 and

TABLE 3. Register Selection for Parallel Output

| POUT_SEL | Normal Register <br> Contents | Floating Point <br> Register <br> Contents |
| :---: | :---: | :---: |
| 0 | IA upper 16-bits | $0000 / \mathrm{elA} / \mathrm{mIA}$ |
| 1 | IA lower 16-bits | $0 \times 0000$ |
| 2 | QA upper 16-bits | $0000 / \mathrm{eQA} / \mathrm{mQA}$ |
| 3 | QA lower 16-bits | $0 \times 0000$ |
| 4 | IB upper 16-bits | $0000 / \mathrm{eIB} / \mathrm{mIB}$ |
| 5 | B lower 16-bits | $0 \times 0000$ |
| 6 | QB upper 16-bits | $0000 / \mathrm{eQB} / \mathrm{mQB}$ |
| 7 | QB lower 16-bits | $0 \times 0000$ |

all other bits are set to zero. For the floating point format, the valid bits are placed in the upper 16-bits of the appropriate channel register using the format $0000 / \mathrm{el} / \mathrm{ml}$ for the I samples.

### 6.0 AGC

The LM97593 AGC processor monitors the output level of the ADC and servos it to the desired setpoint. The ADC input is controlled by the DVGA to maintain the proper setpoint level. DVGA operation results in a compression of the signal through the ADC. The DVGA signal compression is reversed in the LM97593 to provide > 120dB of linear dynamic range. This is illustrated in Figure 36.


FIGURE 36. Output Gain Scaling vs. Input Signal
In order to use the AGC, the DRCS Control Panel software may be used to calculate the programmable parameters. To generate these parameters, only the desired setpoint, deadband+ hysteresis, and loop time constant need to be supplied. All subsequent calculations are performed by the software. Complete details of the AGC operation are provided in an appendix.


FIGURE 37. AGC Setup
AGC setpoint and deadband are illustrated in Figure 37. The loop time constant is a measure of how fast the loop will track
a changing signal. Values down to approximately $1.0 \mathrm{mi}-$ crosecond will be stable with the second order LC noise filter. Since the DVGA operates with 6dB steps the deadband should always be greater than 6 dB to prevent oscillation. An increased deadband value will reduce the amount of AGC operation. A decreased deadband value will increase the amount of AGC operation but will hold the ADC output closer to the setpoint. The threshold should be set so that transients do not cause sustained overrange at the ADC inputs. The threshold setting can also be used to set the ADC input near its optimal performance level.
The AGC will free run when AGC_HOLD_IC is set to ' 0 '. It may be set to a fixed gain by setting AGC_HOLD_IC to ' 1 ' after programming the desired gain in the AGC_IC_A and AGC_IC_B registers. Allowing the AGC to free run should be appropriate for most applications.
Programming the AGC_COMB_ORD register allows the AGC power detector bandwidth to be reduced if desired. This will tend to improve the power detector's ability to reject the signal carrier frequency and reduce overall AGC activity. Figure 39 shows the power detector response.
The analog gain change from the DVGA must be compensated by the "Float To Fixed" converter after the appropriate delay. This delay can be adjusted by the EXT_DELAY register value to make sure the analog gain change is properly compensated in the digital domain.
Figure 38 shows the internal clock latency paths related to the DVGA and "Float To Fixed" timing conpensation. In this diagram registers are represented by $z^{-N}$ where N is the sample delay in ADC clock periods. Following the path from the output of the AGC integrator through the DVGA, bandpass filter, ADC and internal register delays adds up to 6 clocks prior to the "Float To Fixed" converter excluding the bandpass filter and ADC. Following the path from the AGC integrator to the "Float To Fixed" is also 6 clocks when EXT_DELAY $=0$. The value programmed in EXT_DELAY should be set to the pipeline latency of the ADC plus the latency of the bandpass filter (typically one clock). If ASTROBE and BSTROBE are not used then subtract one from the resulting total latency.
The LM97593 includes an integrated ADC with a pipeline latency of 7 clocks. Adding one additional clock period for the bandpass filter requires EXT_DELAY $=7$ when the DVGA ASTROBE and BSTROBE signals are used, otherwise, program EXT_DELAY = 6. In most cases ASTROBE and BSTROBE signals are not used so EXT_DELAY is typically set to 6.
More accurate time alignment may improve the equalizer / demodulator performance for EDGE modulated signals and other signals with a large AM component.

### 7.0 POWER MANAGEMENT

The LM97593 can be placed in a low power (static) state by stopping the input clock and setting the PD pin high. To prevent this from placing the LM97593 into unexpected states, the $\overline{\mathbf{S I}}$ pin of the LM97593 should be asserted prior to disabling the input clock and held asserted until the input clock has returned to a stable condition.

### 8.0 TESTABILITY

### 8.1 JTAG Boundary Scan

The LM97593 supports IEEE 1149.1 compliant JTAG Boundary Scan for the I/O's. The following pins are used:

| TRST | (test reset) |
| :--- | :--- |
| TMS | (test mode select) |
| TDI | (test data in) |
| TDO | (test data out) |
| TCK | (test clock) |

The following JTAG instructions are supported:

| Instruction | Description |
| :--- | :--- |
| BYPASS | Connects TDI directly to TDO |
| EXTEST | Enables the test access port <br> controller to drive the outputs |
| IDCODE | Connects the 32-bit ID register to <br> TDO |
| SAMPLE/PRELOAD | Allows the test access port to <br> sample the device inputs and <br> preload test output data |
| HIGHZ | Tri-states the outputs |

The JTAG Boundary Scan can be used to verify printed circuit board continuity at the system level.

### 8.2 Test Register

The user is able to program a value into TEST_REG and substitute this for the normal channel inputs from the AIN/ BIN pins by selecting it with the crossbar. With the NCO frequency set to zero this allows the DDCs and the output
interface of the chip to be verified. Also, the AGC loop can be opened by setting AGC_HOLD_IC high and setting the gain of the DVGA by programming the appropriate value into the AGC_IC_A/B register.

### 8.3 Debug Access Port

Real-time access to the following signals is provided by configuring the control interface debug register:

- NCO sine and cosine outputs
- data after round following mixers
- data before F1 and F2
- data after CIC filter within the AGC

The access points are multiplexed to a 20 -bit parallel output port which is created from signal pins POUT[15:0], AOUT, BOUT, SFS, and RDY according to the table below:

| Normal Mode Pin | Debug Mode Pin |
| :--- | :--- |
| POUT[15:0] | DEBUG[19:4] |
| RDY | DEBUG[3] |
| SFS | DEBUG[2] |
| AOUT | DEBUG[1] |
| BOUT | DEBUG[0] |

SCK will be set to the proper strobe rate for each debug tap point. $\overline{\text { POUT_EN }}$ and PSEL[2:0] have no effect in Debug Mode. The outputs are turned on when the Debug Mode bit is set. Normal serial outputs are also disabled.

### 9.0 CONTROL REGISTERS

The chip is configured and controlled through the use of 8-bit control registers. These registers are accessed for reading or writing using the control bus pins ( $\overline{\mathrm{CE}}, \overline{\mathrm{RD}}, \overline{\mathrm{WR}}, \mathrm{A}[7: 0]$, and D [7:0]) described in section 3.0 Control Interface.
The two sets of FIR coefficients are overlaid at the same memory address. Use the PAGE_SEL registers to access the second set of coefficients.
The register names and descriptions are listed below in section 9.1 Control Register Addresses and Defaults. A quick reference table is provided in the Condensed LM97593 Address Map.

### 9.1 Control Register Addresses and Defaults

| Register Name | Width | Type | Defaulta | Addr | Bit | Description |
| :--- | :---: | :---: | :---: | :---: | :---: | :--- |
| DEC | 11b | R/W | 7 | 0(LSBs) <br> 1(MSBs) | $7: 0$ <br> $2: 0$ | CIC decimation control. N=DEC+1. Valid range is from 7 to <br> 2047. Format is an unsigned integer. This affects both channels. |
| DEC_BY_4 | 1b | R/W | 0 | 1 | 4 | Controls the decimation factor in F2. 0=Decimate by 2. <br> 1=Decimate by 4. This affects both channels. |
| SCALE | 6b | R/W | 0 | 2 | $5: 0$ | CIC SCALE parameter. Format is an unsigned integer <br> representing the number of left bit shifts to perform on the data <br> prior to the CIC filter. Valid range is from 0 to 40. This affects <br> both channels. |
| GAIN_A | 3b | R/W | 0 | 3 | $2: 0$ | Value of left bit shift prior to F1 for channel A. |
| GAIN_B | 3b | R/W | 0 | 4 | $2: 0$ | Value of left bit shift prior to F1 for channel B. |
| RATE | 1B | R/W | 1 | 5 | $7: 0$ | Determines rate of serial output clock. The output rate is FCK/ <br> (RATE+1). Unsigned integer values of 0, 1, 3, 7, 15, and 31 are <br> allowed. |
| SOUT_EN | 1b | R/W | 0 | 6 | 0 | Enables the serial output pins AOUT, BOUT, SCK, and SFS. <br> 0=Tristate. 1=Enabled. |
| SCK_POL | 1b | R/W | 0 | 6 | 1 | Determines polarity of the SCK output. 0=AOUT, BOUT, and <br> SFS change on the rising edge of SCK (capture on falling edge). <br> 1=They change on the falling edge of SCK. |


| Register Name | Width | Type | Default | Addr | Bit | Description |
| :--- | :---: | :---: | :---: | :---: | :---: | :--- |
| SFS_POL | 1b | R/W | 0 | 6 | 2 | Determines polarity of the SFS output. 0=Active High. 1=Active <br> Low. |
| RDY_POL | 1 b | R/W | 0 | 6 | 3 | Determines polarity of the RDY output. 0=Active High. 1=Active <br> Low. |
| MUX_MODE | 1 b | R/W | 0 | 6 | 4 | Determines the mode of the serial outputs. 0=Each channel is <br> output on its respective pin, $1=$ Both channels are multiplexed <br> and output on AOUT. See also . |
| PACKED | 1 l | R/W | 0 | 6 | 5 | Controls when SFS goes active. 0=SFS pulses prior to the start <br> of the I and the Q words. 1=SFS pulses only once prior to the <br> start of each I/Q sample pair (i.e. the pair is treated as a double- <br> sized word) The I word precedes the Q word. See. |


| Register Name | Width | Type | Defaulta | Addr | Bit | Description |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| FORMAT | 2b | R/W | 0 | 6 | 7:6 | Determines output number format. $0=$ Truncate serial output to 8 bits. Parallel output is truncated to 32 bits. $1=$ Round both serial and parallel to 16 -bits. All other bits are set to $0.2=$ Round both serial and parallel to 24 -bits. All other bits are set to $0.3=$ Output floating point. 8 -bit mantissa, 4 -bit exponent. All other bits are set to 0 . |
| FREQ_A | 4B | R/W | 0 | 7-10 | 7:0 | Frequency word for channel A. Format is a 32-bit, 2's complement number spread across 4 registers. The LSBs are in the lower registers. The NCO frequency $F$ is $F / F_{C K}=F R E Q \_A /$ 232. |
| PHASE_A | 2B | R/W | 0 | 11-12 | 7:0 | Phase word for channel A. Format is a 16-bit, unsigned magnitude number spread across 2 registers. The LSBs are in the lower registers. The NCO phase PHI is $\mathrm{PHI}=2^{*} \mathrm{p} \mathrm{i}^{*}$ PHASE_A/ 216. |
| FREQ_B | 4B | R/W | 0 | 13-16 | 7:0 | Frequency word for channel B. Format is a 32-bit, 2's complement number spread across 4 registers. The LSBs are in the lower registers. The NCO frequency $F$ is $F / F_{C K}=F R E Q \_B /$ 232. |
| PHASE_B | 2B | R/W | 0 | 17-18 | 7:0 | Phase word for channel B. Format is a 16-bit, unsigned magnitude number spread across 2 registers. The LSBs are in the lower registers. The NCO phase PHI is $\mathrm{PHI}=2^{*} \mathrm{pi}^{*} \mathrm{PHASE}$ _B/ $2^{16}$. |
| A_SOURCE | 2 | R/W | 0 | 19 | 1:0 | $0=$ Select AIN as channel input source. 1=Select BIN. 2=3=Select TEST_REG as channel input source. |
| B_SOURCE | 2 | R/W | 1 | 19 | 3:2 | $0=$ Select AIN as channel input source. 1=Select BIN. 2=3=Select TEST_REG as channel input source. |
| EXP_INH | 1b | R/W | 0 | 20 | 0 | 0=Allow exponent to pass into FLOAT TO FIXED converter. 1=Force exponent in DDC channel to a 7 (maximum digital gain). This affects both channels. |
| Reserved | 1b | R/W | 1 | 20 | 1 | AGC_FORCE on the CLC5902. Do not use. |
| Reserved | 1b | R/W | 0 | 20 | 2 | AGC_RESET_EN on the CLC5902. Do not use. |
| AGC_HOLD_IC | 1b | R/W | 0 | 20 | 3 | 0=Normal closed-loop operation. 1=Hold integrator at initial condition. This affects both channels. |
| AGC_LOOP_GAIN | 2b | R/W | 0 | 20 | 4:5 | Bit shift value for AGC loop. Valid range is from 0 to 3. This affects both channels. |
| Reserved | 2B | R/W | 0 | 21-22 | 7:0 | AGC_COUNT on the CLC5902. Do not use. |
| AGC_IC_A | 1B | R/W | 0 | 23 | 7:0 | AGC fixed gain for channel $A$. Format is an 8-bit, unsigned magnitude number. The channel A DVGA gain will be set to the inverted three MSBs. |


| Register Name | Width | Type | Default ${ }^{\text {a }}$ | Addr | Bit | Description |
| :--- | :---: | :---: | :---: | :---: | :---: | :--- |
| AGC_IC_B | 1B | R/W | 0 | 24 | $7: 0$ | AGC fixed gain for channel B. Format is an 8-bit, unsigned <br> magnitude number. The channel B DVGA gain will be set to the <br> inverted three MSBs. |
| AGC_RB_A | 1B | R | 0 | 25 | $7: 0$ | AGC integrator readback value for channel A. Format is an 8- <br> bit, unsigned magnitude number. The user can read the <br> magnitude MSBs of the channel A integrator from this register. |
| AGC_RB_B | 1B | R | 0 | 26 | $7: 0$ | AGC integrator readback value for channel B. Format is an 8- <br> bit, unsigned magnitude number. The user can read the <br> magnitude MSBs of the channel B integrator from this register. |
| TEST_REG | $14 b$ | R/W | 0 | 27(LSBs) <br> $28(M S B s)$ | $7: 0$ <br> $5: 0$ | Test input source. Instead of processing values from the <br> AlBIN pins, the value from this location is used instead. Format <br> is 14-bit 2s complement number spread across 2 registers. |
| Reserved | 1B | - | - | 29 | $7: 0$ | For future use. |


| Register Name | Width | Type | Defaulta | Addr | Bit | Description |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Reserved | 1B | - |  | 30 | 7:0 | For future use |
| DEBUG_EN | 1b | R/W | 0 | 31 | 0 | 0=Normal. 1=Enables access to the internal probe points. |
| DEBUG_TAP | 5b | R/W | 0 | 31 | 5:1 | Selects internal node tap for debug. 0 selects F 1 output for $\mathrm{BI}, 20$ bits 1 selects F1 output for $B Q, 20$ bits 2 selects F1 output for AQ, 20 bits 3 selects F1 output for AI, 20 bits 4 selects F 1 input for $\mathrm{BI}, 20$ bits 5 selects F1 input for BQ, 20 bits 6 selects F1 input for AI, 20 bits 7 selects $F$ 1 input for $A Q$, 20 bits 8 selects NCO A, cosine output. 17 bits, 3 LSBs are 0. 9 selects NCO A, sine output, 17 bits, 3 LSBs are 0. 10 selects NCO B, cosine output, 17 bits, 3 LSBs are 0. 11 selects NCO B, sine output, 17 bits, 3 LSBs are 0. 12 selects NCO AI, rounded output, 15 bits, 5 LSBs are 0. 13 selects NCO AQ, rounded output, 15 bits, 5 LSBs are 0. 14 selects NCO BI, rounded output, 15 bits, 5 LSBs are 0. 15 selects NCO BQ, rounded output, 15 bits, 5 LSBs are 0 . 16 selects AGC CIC filter output. 9 MSBs from ch A, next 9 bits from ch B, 2 LSBs are 0 . <br> 17-31 Reserved. |
| DITH_A | 1b | R/W | 1 | 31 | 6 | 0=Disable NCO dither source for channel A. 1=Enable. |
| DITH_B | 1b | R/W | 1 | 31 | 7 | 0=Disable NCO dither source for channel B. 1=Enable. |
| AGC_TABLE | 32B | R/W | 0 | 128-159 | 7:0 | RAM space that defines key AGC loop parameters. Format is 32 separate 8 -bit, 2's complement numbers. This is common to both channels. |
| F1_COEFF | 22B | R/W | 0 | 160-181 | 7:0 | Coefficients for F1. Format is 11 separate 16-bit, 2's complement numbers, each one spread across 2 registers. The LSBs are in the lower registers. For example, coefficient h0[7:0] is in address 160, h0[15:8] is in address 161, $\mathrm{h} 1[7: 0$ ] is in address 162, h1[15:8] is in address 163. PAGE_SEL_F1=1 maps these addresses to coefficient memory B. |
| F2_COEFF | 64B | R/W | 0 | 182-245 | 7:0 | Coefficients for F2. Format is 32 separate 16-bit, 2's complement numbers, each one spread across 2 registers. The LSBs are in the lower registers. For example, coefficient h0[7:0] is in address 182, h0[15:8] is in address 183, h1[7:0] is in address 184, h1[15:8] is in address 185. PAGE_SEL_F2=1 maps these addresses to coefficient memory B. |


|  |  |  |  |  |  |  |  | Register Name | Width | Type | Defaulta | Addr | Bit | Description |
| :--- | :---: | :---: | :---: | :---: | :---: | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| COEF_SEL_F1A | 1b | R/W | 0 | 246 | 0 | Channel A F1 coefficient select register. 0=memory A, <br> 1=memory B. |  |  |  |  |  |  |  |  |
| COEF_SEL_F1B | 1b | R/W | 0 | 246 | 1 | Channel B F1 coefficient select register. 0=memory A, <br> 1=memory B. |  |  |  |  |  |  |  |  |
| PAGE_SEL_F1 | 1b | R/W | 0 | 246 | 2 | F1 coefficient page select register. 0=memory A, 1=memory B. |  |  |  |  |  |  |  |  |
| COEF_SEL_F2A | 1b | R/W | 0 | 247 | 0 | Channel A F2 coefficient select register. 0=memory A, <br> $1=$ memory B. |  |  |  |  |  |  |  |  |
| COEF_SEL_F2B | 1b | R/W | 0 | 247 | 1 | Channel B F2 coefficient select register. 0=memory A, <br> $1=$ memory B. |  |  |  |  |  |  |  |  |
| PAGE_SEL_F2 | 1b | R/W | 0 | 247 | 2 | F2 coefficient page select register. 0=memory A, 1=memory B. |  |  |  |  |  |  |  |  |
| SFS_MODE | 1b | R/W | 0 | 248 | 0 | 0=SFS asserted at the start of each output word when <br> PACKED=1 or each I/Q pair when PACKED=0, 1=SFS asserted <br> at the start of each output sample period. |  |  |  |  |  |  |  |  |


| Register Name | Width | Type | Defaulta | Addr | Bit | Description |
| :--- | :---: | :---: | :---: | :---: | :---: | :--- |
| SDC_EN | 1b | R/W | 0 | 248 | 1 | 0=normal serial mode, 1=serial daisy-chain master mode. |
| AGC_COMB_ORD | 2b | R/W | 0 | 249 | $1: 0$ | Enable reduced bandwidth AGC power detector. 0=2nd-order <br> decimate-by-eight CIC, 1=1-tap comb added to CIC, 2=4-tap <br> comb added to CIC. |
| EXT_DELAY | 5b | R/W | 0 | 249 | $6: 2$ | Number of CK period delays needed to align the DVGA gain <br> step with the digital gain compensation step. Set this register to <br> 7 if $\overline{\text { ASTROBE and BSTROBE are not used. Otherwise set to 8. }}$. |

a. These are the default values set by a master reset $(\overline{\mathbf{M R}})$. Sync in $(\overline{\mathbf{S I}})$ will not affect any of these values.

### 9.2 Condensed LM97593 Address Map

| Register Name | Addr | Addr <br> Hex | Bit7 | Bit6 | Bit5 | Bit4 | Bit3 | Bit2 | Bit1 | Bit0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DEC | 0 | 0x00 | Dec7 | Dec6 | Dec5 | Dec4 | Dec3 | Dec2 | Dec1 | Dec0 |
| DEC_BY_4 | 1 | 0x01 |  |  |  | DecBy4 |  | Dec10 | Dec9 | Dec8 |
| SCALE | 2 | $0 \times 02$ |  |  | Sc5 | Sc4 | Sc3 | Sc2 | Sc1 | Sc0 |
| GAIN_A | 3 | 0x03 |  |  |  |  |  | GA2 | GA1 | GAO |
| GAIN_B | 4 | 0x04 |  |  |  |  |  | GB2 | GB1 | GB0 |
| RATE | 5 | 0x05 | Rate7 | Rate6 | Rate5 | Rate4 | Rate3 | Rate2 | Rate1 | Rate0 |
| SERIAL_CTRL | 6 | $0 \times 06$ | FMT1 | FMT0 | Packed | MuxMode | RDY_POL | SFS_POL | SCK_POL | SOUT_EN |
| FREQ_A | 7 | 0x07 | FA7 | FA6 | FA5 | FA4 | FA3 | FA2 | FA1 | FAO |
|  | 8 | 0x08 | FA15 | FA14 | FA13 | FA12 | FA11 | FA10 | FA9 | FA8 |
|  | 9 | 0x09 | FA23 | FA22 | FA21 | FA20 | FA19 | FA18 | FA17 | FA16 |
|  | 10 | 0x0A | FA31 | FA30 | FA29 | FA28 | FA27 | FA26 | FA25 | FA24 |
| PHASE_A | 11 | 0x0B | PA7 | PA6 | PA5 | PA4 | PA3 | PA2 | PA1 | PA0 |
|  | 12 | 0x0C | PA15 | PA14 | PA13 | PA12 | PA11 | PA10 | PA9 | PA8 |
| FREQ_B | 13 | 0x0D | FB7 | FB6 | FB5 | FB4 | FB3 | FB2 | FB1 | FB0 |
|  | 14 | 0x0E | FB15 | FB14 | FB13 | FB12 | FB11 | FB10 | FB9 | FB8 |
|  | 15 | 0x0F | FB23 | FB22 | FB21 | FB20 | FB19 | FB18 | FB17 | FB16 |
|  | 16 | 0x10 | FB31 | FB30 | FB29 | FB28 | FB27 | FB26 | FB25 | FB24 |
| PHASE_B | 17 | 0x11 | PB7 | PB6 | PB5 | PB4 | PB3 | PB2 | PB1 | PB0 |
|  | 18 | 0x12 | PB15 | PB14 | PB13 | PB12 | PB11 | PB10 | PB9 | PB8 |
| Source | 19 | 0x13 |  |  |  |  | BS1 | BS0 | AS1 | AS0 |
| AGC_CTRL | 20 | 0x14 |  |  | AgcLG1 | AgcLG0 | AgcHIdIC | Reserved | Reserved | Explnh |
| AGC_COUNT | 21 | 0x15 | Reserved | Reserved | Reserved | Reserved | Reserved | Reserved | Reserved | Reserved |
|  | 22 | 0x16 | Reserved | Reserved | Reserved | Reserved | Reserved | Reserved | Reserved | Reserved |


| Register <br> Name | Addr | Addr <br> Hex | Bit7 | Bit6 | Bit5 | Bit4 | Bit3 | Bit2 | Bit1 | Bit0 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AGC_IC_A | 23 | $0 \times 17$ | AgclcA7 | AgclcA6 | AgclcA5 | AgclcA4 | AgclcA3 | AgclcA2 | AgclcA1 | AgclcA0 |
| AGC_IC_B | 24 | $0 \times 18$ | AgclcB7 | AgclcB6 | AgclcB5 | AgclcB4 | AgclcB3 | AgclcB2 | AgclcB1 | AgclcB0 |
| AGC_RB_A | 25 | $0 \times 19$ | AgcRbA7 | AgcRbA6 | AgcRbA5 | AgcRbA4 | AgcRbA3 | AgcRbA2 | AgcRbA1 | AgcRbA0 |
| AGC_RB_B | 26 | 0x1A | AGCRbB7 | AGCRbB6 | AGCRbB5 | AGCRbB4 | AGCRbB3 | AGCRbB2 | AGCRbB1 | AGCRbB0 |
| TEST_REG | 27 | 0x1B | Test7 | Test6 | Test5 | Test4 | Test3 | Test2 | Test1 | Test0 |
|  | 28 | 0x1C |  |  | Test13 | Test12 | Test11 | Test10 | Test9 | Test8 |
| DEBUG | 31 | 0x1F | DITH_B | DITH_A | TapSel4 | TapSel3 | TapSel2 | TapSel1 | TapSel0 | DebugEnable |
| AGC_TABLE | 128 | 0x80 | The AGC Table loads from the low address to the high address in this order: |  |  |  |  |  |  |  |
|  | 159 | 0x9F | "1st location, 2nd location..." |  |  |  |  |  |  |  |


| Register Name | Addr | Addr Hex | Bit7 | Bit6 | Bit5 | Bit4 | Bit3 | Bit2 | Bit1 | Bit0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F1_COEFF | 160 | 0xA0 |  | The FIR Coefficients load from the low address to the high address in this order: "1st location low byte, 1st location high byte, 2nd location..."" The Page Select bits determine which set of coefficient memory is written. |  |  |  |  |  |  |
|  | 181 | 0xB5 |  |  |  |  |  |  |  |  |
| F2COEFF | 182 | 0xB6 |  |  |  |  |  |  |  |  |
|  | 245 | 0xF5 |  |  |  |  |  |  |  |  |
| F1_CTRL | 246 | 0xF6 |  |  |  |  |  | PgSelF1 | CfSelF1B | CfSelF1A |
| F2_CTRL | 247 | 0xF7 |  |  |  |  |  | PgSelF2 | CfSelF2B | CfSelF2A |
| SERIAL_CTRL2 | 248 | 0xF8 |  |  |  |  |  |  | SdcEn | SfsMode |
| AGC_CTRL2 | 249 | 0xF9 |  | ExtDelay4 | ExtDelay3 | ExtDelay2 | ExtDelay1 | ExtDelay0 | CombOrd1 | CombOrd0 |

## AGC Theory of Operation

A block diagram of the AGC is shown in Figure 40. The DVGA interface comprises four pins for each of the channels. The first three pins of this interface are a 3-bit binary word that controls the DVGA gain in 6dB steps (AGAIN). The final pin is $\overline{\text { ASTROBE }}$ which allows the AGAIN bits to be latched into the DVGA's register. A key feature of the ASTROBE, illustrated Figure 41, is that it toggles only if the data on AGAIN has changed from the previous cycle. Not shown is that $\overline{\text { AS- }}$ TROBE and $\overline{\text { BSTROBE }}$ are independent. For example, $\overline{\text { AS- }}$ TROBE only toggles when AGAIN has changed. BSTROBE will not toggle because AGAIN has changed. This is done to minimize unnecessary digital noise on the sensitive analog path through the DVGA. $\overline{\text { ASTROBE }}$ and $\overline{\text { BSTROBE }}$ are asserted during $\overline{\mathbf{M R}}$ and $\overline{\mathbf{S I}}$ to properly initialize the DVGAs.
The absolute value circuit and the 2 -stage, decimate-by- 8 CIC filter comprise the power detection part of the AGC. The power detector bandwidth is set by the CIC filter to $\mathrm{F}_{\mathrm{CK}} / 8$. The absolute value circuit doubles the effective input frequency. This has the effect of reducing the power detector bandwidth from $\mathrm{F}_{\mathrm{CK}} / 8$ to $\mathrm{F}_{\mathrm{CK}} / 16$.
For a full-scale sinusoidal input, the absolute value circuit output is a dc value of $511^{*}(2 / \pi)$. Because the absolute value
circuit also generates undesired even harmonic terms, the CIC filter (response shown in Figure 39) is required to remove these harmonics. The first response null occurs at


30008736
FIGURE 39. Power detector filter response, 52 MHz


FIGURE 40. LM97593 AGC circuit, Channel A


FIGURE 41. Timing diagram for AGC/DVGA interface, Channel A. Refer to Figure 7 for detailed timing information.
$\mathrm{F}_{\mathrm{CK}} / 8$, where $\mathrm{F}_{\mathrm{CK}}$ is the clock frequency, and the response magnitude is at least 25 dB below the dc value from $\mathrm{F}_{\mathrm{CK}} / 10$ to $9 \mathrm{~F}_{C K} / 10$. Because the $2^{\text {nd }}$ harmonic from the absolute value circuit is about 10 dB below the dc this means that the ripple in the detected level is about 0.7 dB or less for input frequencies between $\mathrm{F}_{\mathrm{CK}} / 20$ to $19 \mathrm{~F}_{\mathrm{CK}} / 20$. Setting the AGC_COMB_ORD register to either 1 or 2 will narrow the power detector's bandwidth as shown in Figure 39.
The "FIXED TO FLOAT CONVERTER" takes the fixed point 9-bit output from the CIC filter and converts it to a "floating point" number. This conversion is done so that the 32 values in the RAM can be uniformly assigned (dB scale) to detected power levels ( 54 dB range). This provides a resolution of 1.7 dB between detected power levels. The truth table for this converter is given in Table 4. The upper three bits of the output represent the exponent (e) and the lower 2 are the mantissa ( m ). The exponent is determined by the position of the leading ' 1 ' out of the CIC filter. An output of ' 001 XX ' corresponds to a leading ' 1 ' in bit 2 (LSB is bit 0 ). The exponent increases by one each time the leading ' 1 ' advances in bit position. The mantissa bits are the two bits that follow the leading ' 1 '. If we define $E$ as the decimal value of the exponent bits and M as the decimal value of the mantissa bits, the output of the CIC filter, POUT, corresponding to a given "FIXED TO FLOAT CONVERTER" output is:

$$
\begin{align*}
& P_{\text {OUT }}= {[4 * \min (E, 1)+M] . } \\
& 2^{(\max (E, 1)-1)}, E \geq 1 . \tag{Eq.9}
\end{align*}
$$

The $\max ()$ and $\min ()$ operators account for row 1 of Table 4 which is a special case because $\mathrm{M}=\mathrm{P}_{\text {out }}$. Equation 5 associates each address of the RAM with a CIC filter output.

TABLE 4. Fixed to Float Converter Truth Table

| INPUT | OUTPUT (eeemm) |
| :---: | :---: |
| $0-3$ | $000 X X$ |
| $4-7$ | 001 XX |
| $8-15$ | 010 XX |
| $16-31$ | 011 XX |
| $32-63$ | 100 XX |
| $64-127$ | 101 XX |
| $128-255$ | $110 X X$ |
| $256-511$ | 111 XX |

As shown in Figure 40, the 32X8 RAM look-up table implements the functions of log converter, reference subtraction, error amplifier, and deadband. The user must build each of these functions by constructing a set of 8-bit, 2's complement numbers to be loaded into the RAM. Each of these functions and how to construct them are discussed in the following paragraphs.
A log conversion is done in order to keep the loop gain independent of operating point. To see why this is beneficial, the control gain of the DVGA computed without log conversion is:

$$
\begin{gather*}
K_{D V G A}^{\prime}=\frac{\partial}{\partial G}\left(v_{i} \cdot 2^{\left(G-G_{o}\right)}\right),  \tag{Eq.10}\\
\quad=-v_{i} \cdot \ln (2) \cdot 2^{\left(G-G_{o}\right)}
\end{gather*}
$$

where $G$ is the decimal equivalent of GAIN and $G_{o}$ accounts for the DVGA gain in excess of unity. This equation assumes
that the DVGA gain control polarity is positive as is the case for the CLC5526. The gain around the entire loop must be negative. Observe in Equation 6 that the control gain is dependent on operating point G. If we instead compute the control gain with log conversion then:

$$
\begin{align*}
K_{D V G A} & =\frac{\partial}{\partial G}\left[20 \cdot \log \left(v_{i} \cdot 2^{\left(G-G_{o}\right)}\right)\right],  \tag{Eq.11}\\
& =-6.02,
\end{align*}
$$

which is no longer operating-point dependent. The log function is constructed by computing the CIC filter output associated with each address (Equation 5) and converting these to dB . Full scale (dc signal) is $20 \log (511)=54 \mathrm{~dB}$.
The reference subtraction is constructed by subtracting the desired loop servo point (in dB ) from the table values computed in the previous paragraph. For example, if it is desired that the DVGA servo the ADC input level (sinusoidal signal) to -6 dBFS , the number to subtract from the data is:

$$
\begin{equation*}
20 \log \left(\frac{511}{2} \cdot \frac{2}{\pi}\right)=44 d B \tag{Eq.12}
\end{equation*}
$$

The table data will then cross through zero at the address corresponding to this reference level. A deadband wider than 6 dB should then be constructed symmetrically about this point. This prevents the loop from hunting due to the 6 dB gain steps of the DVGA. Any deadband in excess of 6 dB appears as hysteresis in the servo point of the loop as illustrated in Figure 37. The deadband is constructed by loading zeros into those addresses on either side of the one which corresponds to the reference level.
The last function of the RAM table is that of error amplification. All the operations preceding this one gave a table slope $S_{\text {RAM }}=1$. This must now be adjusted in order to control the time constant of the loop given by:

$$
\begin{equation*}
\tau=\frac{8}{F_{C K}}\left(\frac{1}{G_{L}}+\frac{1}{2}\right) \tag{Eq.13}
\end{equation*}
$$

The term $G_{L}$ in this equation is the loop gain:

$$
\begin{equation*}
G_{L}=-6.02 \cdot S_{R A M} \cdot 2^{\left(A G C_{-} L O O P P_{-} G A I N-8\right)} . \tag{Eq.14}
\end{equation*}
$$

The design equations are obtained by solving Equation 13 for $G_{L}$ and Equation 14 for $S_{\text {RAM }}$. AGC_LOOP_GAIN is a control register value that determines the number of bits to shift the output of the RAM down by. This allows some of the loop gain to be moved out of the RAM so that the full output range of the table is utilized but not exceeded. The valid range for AGC_LOOP_GAIN is from 0 to 3 which corresponds to a 0 to 3 bit shift to the left.
An example set of numbers to implement a loop having a reference of 6 dB below full scale, a deadband of 8 dB , and a loop gain of 0.108 is:

- 102-102-88-80-75-70-86
-63-61-56-53-50
-47-42-39 -36-33-29 -25
-22-19-15-11-0
00000131720


30008739


30008740
FIGURE 43. Example of programmed RAM contents

FIGURE 42. Example of programmed RAM contents

TABLE 5. 15-bit Mixer Output Alignment into the 22-bit SHIFT-UP Based On EXP

| AGAINa | EXPb | Input $\mathbf{c}$ | $\mathbf{2 1 d}^{\mathrm{d}}$ | $\mathbf{2 0}$ | $\mathbf{1 9}$ | $\mathbf{1 8}$ | $\mathbf{1 7}$ | $\mathbf{1 6}$ | $\mathbf{1 5}$ | $\mathbf{1 4}$ | $\ldots$ | $\mathbf{8}$ | $\mathbf{7}$ | $\mathbf{6}$ | $\mathbf{5}$ | $\mathbf{4}$ | $\mathbf{3}$ | $\mathbf{2}$ | $\mathbf{1}$ | $\mathbf{0}$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $000=-12 \mathrm{~dB}$ | $111=+0 \mathrm{~dB}$ | -12 dB | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | $\ldots$ | 1 | 0 | L | L | L | L | L | L | L |
| $001=-6 \mathrm{~dB}$ | $110=-6 \mathrm{~dB}$ | -12 dB | 14 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | $\ldots$ | 2 | 1 | 0 | L | L | L | L | L | L |
| $010=0 \mathrm{~dB}$ | $101=-12 \mathrm{~dB}$ | -12 dB | 14 | 14 | 14 | 13 | 12 | 11 | 10 | 9 | $\ldots$ | 3 | 2 | 1 | 0 | L | L | L | L | L |
| $011=+6 \mathrm{~dB}$ | $100=-18 \mathrm{~dB}$ | -12 dB | 14 | 14 | 14 | 14 | 13 | 12 | 11 | 10 | $\ldots$ | 4 | 3 | 2 | 1 | 0 | L | L | L | L |
| $100=+12 \mathrm{~dB}$ | $011=-24 \mathrm{~dB}$ | -12 dB | 14 | 14 | 14 | 14 | 14 | 13 | 12 | 11 | $\ldots$ | 5 | 4 | 3 | 2 | 1 | 0 | L | L | L |
| $101=+18 \mathrm{~dB}$ | $010=-30 \mathrm{~dB}$ | -12 dB | 14 | 14 | 14 | 14 | 14 | 14 | 13 | 12 | $\ldots$ | 6 | 5 | 4 | 3 | 2 | 1 | 0 | L | L |
| $110=+24 \mathrm{~dB}$ | $001=-36 \mathrm{~dB}$ | -12 dB | 14 | 14 | 14 | 14 | 14 | 14 | 14 | 13 | $\ldots$ | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | L |
| $111=+30 \mathrm{~dB}$ | $000=-42 \mathrm{~dB}$ | -12 dB | 14 | 14 | 14 | 14 | 14 | 14 | 14 | 14 | $\ldots$ | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 |

a. AGAIN sets the DVGA or analog gain value.
b. EXP sets the "FIXED TO FLOAT CONVERTER" or digital gain value.
c. 22-bit input to SHIFT-UP block in Figure 19 horizontally, linearized SHIFT-UP value vertically.
d. The numbers in the center of the table represent the mixer output bits. 'L' represents a logic low.

These values are shown with respect to the table addresses in Figure 42, and the CIC filter output $\mathrm{P}_{\text {OUT }}$ in Figure 43. For a 52 MHz clock rate and AGC_LOOP_GAIN=2, these values result in a loop time constant of $1.5 \mu \mathrm{~s}$.
The error signal from the loop gain "SHIFT DOWN" circuit is gated into the loop integrator. A MUX within the integrator feedback allows the integrator to be initialized to the value loaded into AGC_IC_A (channel B can be set independently). The top eight bits of the integrator output can also be read back over the microprocessor interface from the AGC_RB_A (or AGC_RB_B) register. The top 3 bits become AGAIN and are output along with the ASTROBE signal on the DVGA interface pins. The valid range of AGAIN is from 0 to 7 which corresponds to a valid range of 0 to $2^{11-1}$ for the 11-bit, 2's complement integrator output from which AGAIN is derived. This is illustrated in Figure 44. The integrator saturates at these limits to prevent overshoots as the integrator attempts to enter the valid range. The AGAIN value is inverted (EXP)
and used to adjust the gain of the incoming signal to provide a linear output dynamic range. The relationship between the DVGA analog gain (AGAIN) and the "FIXED TO FLOAT CONVERTER" digital gain (EXP) is shown in Table 5. The DVGA's compression of the incoming signal in the analog domain vs. the subsequent expansion in the digital domain is shown in Figure 36.
The AGC may be forced to free run by setting AGC_HOLD_IC low. Writing an initial condition to AGC_IC_AIB and then setting AGC_HOLD_IC high will force the AGC to a fixed gain. The three MSBs of the value written to AGC_IC_AIB are inverted and output to drive the DVGA.
Allowing the AGC to free run should be appropriate for most applications. If the INH_EXP bit is not set, the DVGA gain word (EXP) is routed to the "FLOAT TO FIXED CONVERTER" in the DDCs prior to the programmable decimation filter. The EXP signals are delayed to account for the propagation delay of the DVGA interface and the ADC12DL080 ADC.

## General Applications Information

### 10.0 OUTPUTS

Be very careful when driving a high capacitance bus. The more capacitance the output drivers must charge for each conversion, the more instantaneous digital current flows through $\mathrm{V}_{\mathrm{DR}}$ and DRGND. These large charging current spikes can cause on-chip ground noise and couple into the analog circuitry, degrading dynamic performance. Adequate bypassing, limiting output capacitance and careful attention to the ground plane will reduce this problem.
To minimize noise due to output switching, minimize the load currents at the digital outputs. Only one driven input should be connected to each output pin. Additionally, inserting series resistors of about $100 \Omega$ at the digital outputs, close to the ADC pins, will isolate the outputs from trace and other circuit capacitances and limit the output currents, which could otherwise result in performance degradation. See Figure 45.

FIGURE 44. AGC integrator output limits

| FILTER COMPONENT VALUES |  |  |
| :---: | :---: | :---: |
|  | FREQUENCY |  |
|  | 150 MHz | 250 MHz |
| L 1 | 43 nH | 22 nH |
| C 1 | 43 pF | 18 pF |
| C 2 | 43 pF | 18 pF |
| C 3 | - | 0.5 pF |

Note:
$\rightarrow$ PCB parasitics may require component value adjustment.
$\rightarrow$ See LM97593 EB user's guide for complete details.

FIGURE 45. Application Circuit

### 11.0 POWER SUPPLY CONSIDERATIONS

The power supply pins should be bypassed with a $10 \mu \mathrm{~F}$ capacitor and with a $0.1 \mu \mathrm{~F}$ ceramic chip capacitor near each power pin. Leadless chip capacitors are preferred because they have low series inductance.
The LM97593 is sensitive to power supply noise. Accordingly, the noise on the analog supply pins should be kept below 100 $m V_{\text {P-p }}$.
No pin should ever have a voltage on it that is in excess of the supply voltages, not even on a transient basis. Be especially careful of this during power turn on and turn off.
The $V_{D R}$ pin provides power for the output drivers and should be operated from a supply equivalent to $V_{D}$.

### 12.0 LAYOUT AND GROUNDING

A proper grounding and proper routing of all signals are essential to ensure accurate conversion. Maintaining separate analog and digital areas of the board, with the LM97593 between these areas, is required to achieve specified performance.
The ground return for the data outputs (DRGND) carries the ground current for the output drivers. The output current can exhibit high transients that could add noise to the conversion process. To prevent this from happening, the DRGND pins should NOT be connected to system ground in close proximity to any of the LM97593's other ground pins.
Capacitive coupling between the typically noisy digital circuitry and the sensitive analog circuitry can lead to poor performance. The solution is to keep the analog circuitry separated from the digital circuitry, and to keep the clock line as short as possible.
Digital circuits create substantial supply and ground current transients. The logic noise thus generated could have significant impact upon system noise performance. The best logic family to use in systems with A/D converters is one which employs non-saturating transistor designs, or has low noise characteristics, such as the $74 \mathrm{LS}, 74 \mathrm{HC}(\mathrm{T})$ and $74 \mathrm{AC}(\mathrm{T}) \mathrm{Q}$ families. The worst noise generators are logic families that create the largest supply current transients during clock or signal edges, like the 74F and the 74AC(T) families.
The effects of the noise generated from the LM97593 output switching can be minimized through the use of $100 \Omega$ resistors in series with each data output line. Locate these resistors as close to the LM97593 output pins as possible.
Since digital switching transients are composed largely of high frequency components, total ground plane copper weight will have little effect upon the logic-generated noise. This is because of the skin effect. Total surface area is more important than is total ground plane volume.
Generally, analog and digital lines should cross each other at $90^{\circ}$ to avoid crosstalk. To maximize accuracy in high speed, high resolution systems, however, avoid crossing analog and digital lines altogether. It is important to keep clock lines as short as possible and isolated from ALL other lines, including other digital lines. Even the generally accepted $90^{\circ}$ crossing should be avoided with the clock line as even a little coupling can cause problems at high frequencies. This is because other lines can introduce jitter into the clock line, which can lead to degradation of SNR. Also, the high speed clock can introduce noise into the analog chain.

Best performance at high frequencies and at high resolution is obtained with a straight signal path. That is, the signal path through all components should form a straight line wherever possible.
Be especially careful with the layout of inductors. Mutual inductance can change the characteristics of the circuit in which they are used. Inductors should not be placed side by side, even with just a small part of their bodies beside each other.
The analog input should be isolated from noisy signal traces to avoid coupling of spurious signals into the input. Any external component (e.g., a filter capacitor) connected between the converter's input pins and ground or to the reference input pin and ground should be connected to a very clean point in the ground plane.
All analog circuitry (input amplifiers, filters, reference components, etc.) should be placed in the analog area of the board. All digital circuitry and I/O lines should be placed in the digital area of the board. The LM97593 should be between these two areas. Furthermore, all components in the reference circuitry and the input signal chain that are connected to ground should be connected together with short traces and enter the ground plane at a single, quiet point. All ground connections should have a low inductance path to ground.

### 13.0 DYNAMIC PERFORMANCE

To achieve the best dynamic performance, the clock source driving the CLK input must be free of jitter. Isolate the ADC clock from any digital circuitry with buffers, as with the clock tree shown in Figure 46. The gates used in the clock tree must be capable of operating at frequencies much higher than those used if added jitter is to be prevented.
Best performance will be obtained with a differential input drive, compared with a single-ended drive, as discussed in Sections 1.3.1 and 1.3.2.
It is good practice to keep the clock line as short as possible and to keep it well away from any other signals. Other signals can introduce jitter into the clock signal, which can lead to reduced SNR performance, and the clock can introduce noise into other lines. Even lines with $90^{\circ}$ crossings have capacitive coupling, so try to avoid even these $90^{\circ}$ crossings of the clock line.


FIGURE 46. Isolating the ADC Clock from other Circuitry with a Clock Tree

## Common Application Pitfalls

15.1 Driving the inputs (analog or digital) beyond the power supply rails. For proper operation, all inputs should not go more than 100 mV beyond the supply rails (more than 100 mV below the ground pins or 100 mV above the supply pins). Exceeding these limits on even a transient basis may cause faulty or erratic operation. It is not uncommon for high speed digital components (e.g., 74F and 74AC devices) to exhibit overshoot or undershoot that goes above the power supply or below ground. A resistor of about $47 \Omega$ to $100 \Omega$ in series with any offending digital input, close to the signal source, will eliminate the problem.
Do not allow input voltages to exceed the supply voltage, even on a transient basis. Not even during power up or power down.
Be careful not to overdrive the inputs of the LM97593 with a device that is powered from supplies outside the range of the LM97593 supply. Such practice may lead to conversion inaccuracies and even to device damage.
15.2 Attempting to drive a high capacitance digital data bus. The more capacitance the output drivers must charge for each conversion, the more instantaneous digital current flows through $\mathrm{V}_{\mathrm{DR}}$ and DRGND. These large charging current spikes can couple into the analog circuitry, degrading dynamic performance. Adequate bypassing and maintaining separate analog and digital areas on the pc board will reduce this problem.
The digital data outputs should be buffered (with 74ACQ541, for example) if they will drive a large capacitive load. Dynamic performance can also be improved by adding series resistors at each digital output, close to the LM97593, which reduces the energy coupled back into the part's output pins by limiting the output current. A reasonable value for these resistors is $100 \Omega$.
15.3 Using an inadequate amplifier to drive the analog input. As explained in Section 1.3, the capacitance seen at the input alternates between 8 pF and 7 pF , depending upon the phase of the clock. This dynamic load is more difficult to drive than is a fixed capacitance. If the amplifier exhibits overshoot, ringing, or any evidence of instability, even at a very low level, it will degrade performance. A small series resistor at each amplifier output and a capacitor at the analog inputs will improve performance.

Also, it is important that the signals at the two inputs have exactly the same amplitude and be exactly $180^{\circ}$ out of phase with each other. Board layout, especially equality of the length of the two traces to the input pins, will affect the effective phase between these two signals. Remember that an operational amplifier operated in the non-inverting configuration will exhibit more time delay than will the same device operating in the inverting configuration.
15.4 Operating with the reference pins outside of the specified range. As mentioned in Section 1.2, $\mathrm{V}_{\text {REF }}$ should be in the range of

$$
0.8 \mathrm{~V} \leq \mathrm{V}_{\text {REF }} \leq 1.2 \mathrm{~V}
$$

Operating outside of these limits could lead to performance degradation.
15.5 Inadequate network on Reference Bypass pins $\left(V_{R P} A, V_{R N} A, V_{C O M} A, V_{R P} B, V_{R N} B\right.$ and $\left.V_{C O M} B\right)$. As mentioned in Section 1.2, these pins should be bypassed with 0.1 $\mu \mathrm{F}$ capacitors to ground at $\mathrm{V}_{\mathrm{RM}} \mathrm{A}$ and $\mathrm{V}_{\mathrm{RM}} \mathrm{B}$ and with a $10 \mu \mathrm{~F}$ between pins $V_{R P} A$ and $V_{R N} A$ and between $V_{R P} B$ and $V_{R N} B$ for best performance.
15.6 Using a clock source with excessive jitter, using excessively long clock signal trace, or having other signals coupled to the clock signal trace. This will cause the sampling interval to vary, causing excessive output noise and a reduction in SNR and SINAD performance.

## Evaluation Hardware

Evaluation boards are available to facilitate designs based on the LM97593:

### 16.1 LM97593EB

The LM97593 evaluation board provides a complete narrowband receiver from IF to digital symbols.

### 16.2 SOFTWARE

Control panel software for the LM97593 supports complete device configuration on both evaluation boards.
Integrated capture software manages the capture of data and its storage in a file on a PC.
Matlab script files support data analysis: FFT, DNL, and INL plotting.
This software and additional application information is available on the Basestation CDROM.

Physical Dimensions inches (millimeters) unless otherwise noted


For more National Semiconductor product information and proven design tools, visit the following Web sites at:

| Products |  | Design Support |  |
| :--- | :--- | :--- | :--- |
| Amplifiers | www.national.com/amplifiers | WEBENCH | www.national.com/webench |
| Audio | www.national.com/audio | Analog University | www.national.com/AU |
| Clock Conditioners | www.national.com/timing | App Notes | www.national.com/appnotes |
| Data Converters | www.national.com/adc | Distributors | www.national.com/contacts |
| Displays | www.national.com/displays | Green Compliance | www.national.com/quality/green |
| Ethernet | www.national.com/ethernet | Packaging | www.national.com/packaging |
| Interface | www.national.com/interface | Quality and Reliability | www.national.com/quality |
| LVDS | www.national.com/lvds | Reference Designs | www.national.com/refdesigns |
| Power Management | www.national.com/power | Feedback | www.national.com/feedback |
| Switching Regulators | www.national.com/switchers |  |  |
| LDOs | www.national.com/Ido |  |  |
| LED Lighting | www.national.com/led |  |  |
| PowerWise | www.national.com/powerwise |  |  |
| Serial Digital Interface (SDI) | www.national.com/sdi |  |  |
| Temperature Sensors | www.national.com/tempsensors |  |  |
| Wireless (PLL/VCO) | www.national.com/wireless |  |  |

THE CONTENTS OF THIS DOCUMENT ARE PROVIDED IN CONNECTION WITH NATIONAL SEMICONDUCTOR CORPORATION ("NATIONAL") PRODUCTS. NATIONAL MAKES NO REPRESENTATIONS OR WARRANTIES WITH RESPECT TO THE ACCURACY OR COMPLETENESS OF THE CONTENTS OF THIS PUBLICATION AND RESERVES THE RIGHT TO MAKE CHANGES TO SPECIFICATIONS AND PRODUCT DESCRIPTIONS AT ANY TIME WITHOUT NOTICE. NO LICENSE, WHETHER EXPRESS, IMPLIED, ARISING BY ESTOPPEL OR OTHERWISE, TO ANY INTELLECTUAL PROPERTY RIGHTS IS GRANTED BY THIS DOCUMENT.
TESTING AND OTHER QUALITY CONTROLS ARE USED TO THE EXTENT NATIONAL DEEMS NECESSARY TO SUPPORT NATIONAL'S PRODUCT WARRANTY. EXCEPT WHERE MANDATED BY GOVERNMENT REQUIREMENTS, TESTING OF ALL PARAMETERS OF EACH PRODUCT IS NOT NECESSARILY PERFORMED. NATIONAL ASSUMES NO LIABILITY FOR APPLICATIONS ASSISTANCE OR BUYER PRODUCT DESIGN. BUYERS ARE RESPONSIBLE FOR THEIR PRODUCTS AND APPLICATIONS USING NATIONAL COMPONENTS. PRIOR TO USING OR DISTRIBUTING ANY PRODUCTS THAT INCLUDE NATIONAL COMPONENTS, BUYERS SHOULD PROVIDE ADEQUATE DESIGN, TESTING AND OPERATING SAFEGUARDS.
EXCEPT AS PROVIDED IN NATIONAL'S TERMS AND CONDITIONS OF SALE FOR SUCH PRODUCTS, NATIONAL ASSUMES NO LIABILITY WHATSOEVER, AND NATIONAL DISCLAIMS ANY EXPRESS OR IMPLIED WARRANTY RELATING TO THE SALE AND/OR USE OF NATIONAL PRODUCTS INCLUDING LIABILITY OR WARRANTIES RELATING TO FITNESS FOR A PARTICULAR PURPOSE, MERCHANTABILITY, OR INFRINGEMENT OF ANY PATENT, COPYRIGHT OR OTHER INTELLECTUAL PROPERTY RIGHT.

## LIFE SUPPORT POLICY

NATIONAL'S PRODUCTS ARE NOT AUTHORIZED FOR USE AS CRITICAL COMPONENTS IN LIFE SUPPORT DEVICES OR SYSTEMS WITHOUT THE EXPRESS PRIOR WRITTEN APPROVAL OF THE CHIEF EXECUTIVE OFFICER AND GENERAL COUNSEL OF NATIONAL SEMICONDUCTOR CORPORATION. As used herein:
Life support devices or systems are devices which (a) are intended for surgical implant into the body, or (b) support or sustain life and whose failure to perform when properly used in accordance with instructions for use provided in the labeling can be reasonably expected to result in a significant injury to the user. A critical component is any component in a life support device or system whose failure to perform can be reasonably expected to cause the failure of the life support device or system or to affect its safety or effectiveness.

National Semiconductor and the National Semiconductor logo are registered trademarks of National Semiconductor Corporation. All other brand or product names may be trademarks or registered trademarks of their respective holders.
Copyright© 2008 National Semiconductor Corporation
For the most current product information visit us at www.national.com
National Semiconductor
Americas Technical
Support Center
Email:
new.feedback@nsc.com
Tel: 1-800-272-9959

National Semiconductor Europe Technical Support Center
Email: europe.support @ nsc.com
German Tel: +49 (0) 1805010771 English Tel: +44 (0) 8708504288

National Semiconductor Asia Pacific Technical Support Center Email: ap.support@nsc.com

National Semiconductor Japan
Technical Support Center
Email: jpn.feedback@nsc.com

